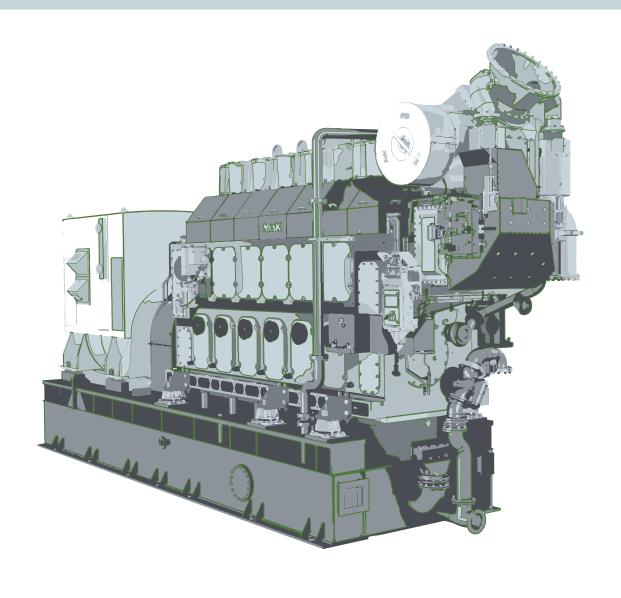
M 46 DF

PROJECT GUIDE / GENERATOR SET







INTRODUCTION

Information for the user of this project guide

The project information contained in the following is not binding, since technical data of products may especially change due to product development and customer requests. Caterpillar reserves the right to modify and amend data at any time. Any liability for accuracy of information provided herein is excluded.

Binding determination of data is made by means of the Technical Specification and such other agreements as may be entered into in connection with the order. We will supply further binding data, drawings, diagrams, electrical drawings, etc. in connection with a corresponding order.

This edition supersedes the previous edition of this project guide.

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Caterpillar Motoren GmbH & Co. KG P. O. Box, D-24157 Kiel Germany

Phone +49 431 3995-01 Telefax +49 431 3995-2193

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INTRODUCTION

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Financial Products: Construction, term and repower financing

Repayment: Loan terms up to 10 years, with longer amortizations available

Financed Amount: Up to 80% of your vessel cost

Rates: Fixed or variable

Currency: US Dollars, Euros and other widely traded currencies

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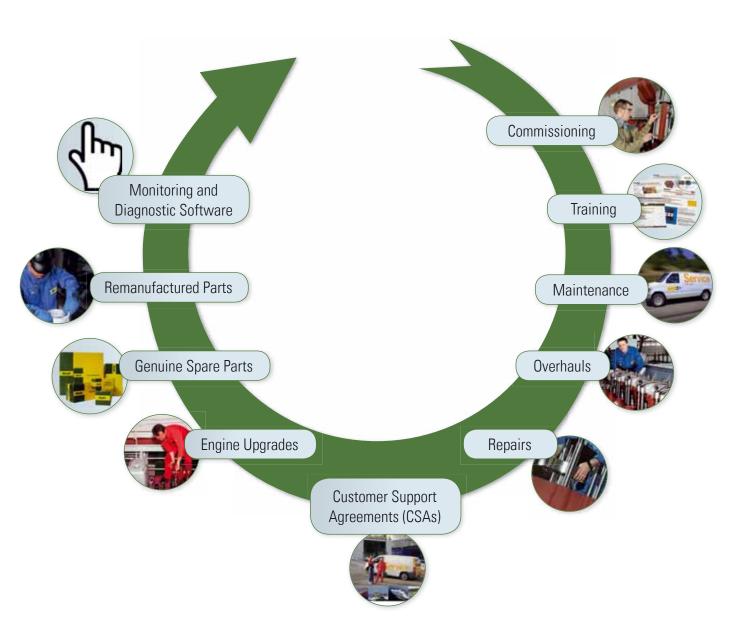








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and the sites

Caterpillar Motoren Rostock GmbH Werftallee 13 18119 Rostock Germany

Caterpillar Motoren Henstedt-Ulzburg GmbH Rudolf-Diesel Straße 5-9 24558 Henstedt-Ulzburg Germany Caterpillar Motoren Guangdong Co. Ltd. Shizhou Industrial Estate Chencun Town Shunde District, Foshan City 528341 P. R. China

has been found to conform to the Management System Standard

ISO 9001:2008

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For Caterpillar Motoren Rostock:
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For Caterpillar Motoren Guangdong:
Production of diesel engines
For Caterpillar Motoren Henstedt-Ulzburg GmbH:
Logistics of spare and serial parts for gas and diesel engines

Initial Certification date:

03.11.2003

This certificate is valid until:

14.11.2016

The audit has been performed under the supervision of

> Stephan Ekat Lead Auditor



Place and date:

Essen, 15.11.2013

for the Accredited Unit: DNV ZERTHIZERUNG UND UMWELTOUTACHTER GMBH

> Nikelaus Kim Management Representative

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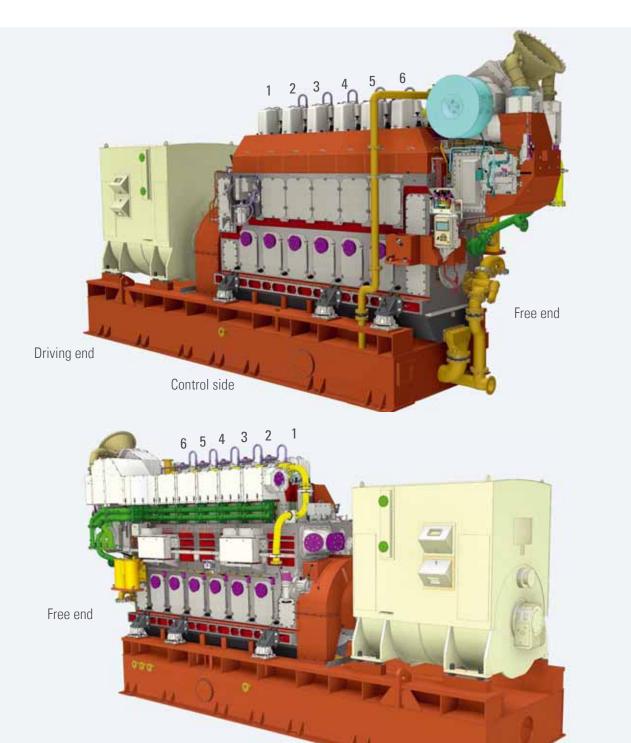


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1.1 Definitions



		6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Output (HFO and MDO)	[kWe]	5,179	6,042	6,905	7,768
Output (MDO only)	[kWe]	5,553	6,478	7,403	8,329

Exhaust side

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Driving end

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Fig. 1-1 M 46 DF

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Cylinder configuration: 6, 7, 8, 9 in-line

Bore: 460 mm Stroke: 610 mm

Output/cyl: 900 kW /965 kW BMEP: 20.7 - 22.8 bar Revolutions: 500/514 rpm Mean piston speed: 10.2/10.5 m/s Single log

Direction of rotation: counter-clockwise, option: clockwise

1.2 Main components and systems

1.2.1 Main features and characteristics

Building on its marine engine legacy Caterpillar Motoren designed the inherently gas safe M 46 DF for a variety of marine applications without sacrificing the typical MaK marine engine attributes like operational reliability and efficiency as well as service and maintenance simplicity.

Capable to operate on multiple fuels (NG/MDO/HFO) the M 46 DF is designed to meet stringent conditions of upcoming exhaust gas emission- and fuel sulphur regulations, providing the operational flexibility for vessel operating in regulated- as well as lesser emission regulated areas.

The optimized design of the M 46 DF in combination with the system solutions provided by Caterpillar Motoren is the basis for the installation and engine/engine room type approval simplicity, reducing changes to engine and engine related systems at the same time.

Low emissions and high engine efficiency, paired with fast service access and service and maintenance simplicity make the MaK M 46 DF the perfect choice for single engine main propulsion installations as well as multiple engine installations.

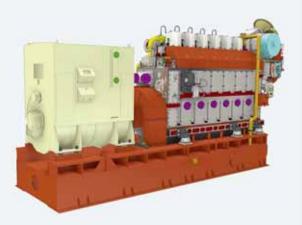


Fig. 1-2 Control side and driving end



Fig. 1-3 Exhaust side and free end

1.2.2 Description of components

Cylinder head

- The cylinder heads are made of nodular cast iron with 2 inlet and 2 exhaust valves, which are equipped with valve rotators.
- The exhaust valve seats are directly water cooled.
- The injection nozzles for heavy fuel operation are cooled by engine lube oil.

Connecting rod and piston

- The pistons are of composite type with steel crown and forged steel or nodular cast iron skirt.
- The piston ring sets consist of two compression rings, first ring with chromium diamond plated running surfaces, the second ring with chromium plated running surfaces, and one chromium diamant plated oil scraper ring.
- All ring grooves are located in the steel crown, which is cooled by lube oil.
- The ring grooves are hardened.
- 3-piece connecting rod, supporting removal of the piston without opening the big end bearing.

Engine block

Core element of the M 46 DF is the engine block, which is made of nodular cast iron in one piece.

The advantages of the engine block design are:

- The one-piece design makes the engine block extremely robust and warp resistant.
- The charge air manifold is cast integral, which avoids vibration and leakage problems.
- Lube oil lines are routed through the block in cast and drilled holes, reducing the number of connecting points and leakage problems to a minimum.
- The camshaft housing contains a camshaft, which is made of sections per cylinder allowing a removal
 of the segments sideways.
- The underslung crankshaft allows the removal of the complete crankshaft without disassembly of the entire engine.
- The engine block is not integrated into the cooling water circuit, therefore the engine block is completely dry.



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Safe and simple power train

The safe and simple designed power train of cylinder head, piston with liner, connecting rod and camshaft is parted in cylinder compartments, while the crankshaft is one-piece. The advantage is simplification of maintenance work saving costs.

Additional advantages are:

- Service friendly distribution of media in maintenance-free plugged pipes and cast blocks
- 2-stage fresh water cooling system with 2-stage charge air cooler
- Turbocharger supplied with inboard plain bearings which are lubricated by engine lube oil
- Service friendly ignition fuel injector location

1.3 Prospective life times

General

The expectable TBO (time between overhaul) and actual life time may deviate significantly as a result of, fuel quality, load and operating profile, conditions, the quality of maintenance and other external factors.

	Life time operating hours [h]					
Core components	M 46 DF Generator Set					
	Gas	MDO	HF0	TB0 M 46 DF		
Piston crown (life time incl. 2 stages rework)		90,000		30,000		
Piston skirt cast iron (standard)		60,000		_		
Piston skirt steel (optional)		90,000		_		
Piston skirt Aluminium		_		_		
Piston rings		30,000		_		
Piston pin bearing		60,000		_		
Cuff / Antipolishing ring		30,000		_		
Cylinder liner	90,	000	60,000	_		
Cylinder head		90,000		15,000		
Inlet valve		30,000		15,000		
Exhaust valve		30,000		15,000		
Nozzle element	7,5	500	5,000	_		
Gas admission valve		7,500		_		
Cylinder pressure sensor		7,500		_		
Pump element		15,000		_		
Pilot injector		7,500		_		
HD-pump		7,500		_		
Main bearing		30,000		_		
Big end bearing		30,000		_		
Camshaft bearing	45,000		_			
Turbocharger plain bearing		12,000		_		
Vibration damper camshaft		15,000		_		
Vibration damper crankshaft		60,000		30,000		

The above mentioned data are only indicative and relate to an average component life time under favourable operating conditions.

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GENERAL DATA AND OUTPUTS

9 M 46 DF

in HFO and MDO mode in MDO mode only 500/514 rpm 500/514 rpm Type [kW] [kW] [kWe] [kWe] 6 M 46 DF 5,400 5,179 5,790 5,553 7 M 46 DF 6,300 6,042 6,755 6,478 8 M 46 DF 7,200 6,905 7,720 7,403

7,768

8,685

8,329

The maximum fuel rack position is mechanically limited to 100 % output for CPP applications.

2.1 General definition of reference conditions

8,100

The maximum continuous rating (locked output) stated by Caterpillar Motoren refers to the following reference conditions according to "IACS" (International Association of Classification Societies) for main and auxiliary engines (tropical conditions):

Air pressure: 100 kPa (1 bar)
Air temperature: 318 K (45 °C)
Relative humidity: 60 %
Seawater temperature: 305 K (32 °C)

2.2 Reference conditions regarding fuel consumption

Fuel consumption data is based on the following reference conditions:

Intake temperature: 298 K (25 °C)
Charge air temperature: 318 K (45°C)
Charge air coolant inlet temperature: 298 K (25°C)
Net heating value of the diesel oil: 42,700 kJ/kg
Net heating value of the natural gas: 43.3 MJ/Nm³

Tolerance: 5 %

Fuel gas minimum lower heating value (LHV): 28.0 MJ/Nm³

Fuel gas methane number for rated output: > 80

Specification of fuel consumption data without engine driven pumps;

For engine driven oil pump: n=const. 1% at 100%, 1.2% at 85%, 1.3% at 75%, 2% at 50%, 4% at 25%. For engine driven cooling water pump: 0.4% at 100%, 0.47% at 85%, 0.53% at 75%, 0.8% at 50%, 1.6% at 25%.

2.3 Lube oil consumption

- 0.6 g/kWh
- Value is based on rated output
- Tolerance ± 0.3 g/kWh

NOTE:

Please also compare the technical data (see chapter 4).

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2.4 Emissions

2.4.1 Exhaust gas 900 kW/Cyl., 500/514 rpm (HFO/MDO) – preliminary

Tolerance: 5 % Relative humidity: 60 % Atmospheric pressure: 100 kPa (1 bar) Constant speed 500/514 rpm

Atmospheric p	oressure:	100 kPa (1 bar) Constant speed 500/514					0/514 rpm			
	Output		Output [%]							
Engine	[kW]		[kg/h] [°C]							
		100	90	80	70	60	50			
Intake air te	emperature	25°C – Dies	el operation							
6 M 46 DF	5,400	39,510 345	36,180 335	32,160 330	28,650 340	24,865 355	21,075 376			
7 M 46 DF	6,300	46,100 343	42,200 350	37,500 345	33,425 350	29,000 360	24,550 385			
8 M 46 DF	7,200	52,675 335	48,725 330	43,310 325	38,585 330	33,485 345	28,380 375			
9 M 46 DF	8,100	59,300 335	54,815 335	48,725 330	43,405 335	37,670 360	31,925 380			
Intake air te	emperature	25°C – Gas	operation							
6 M 46 DF	5,400	33,885 385	31,150 397	27,690 400	25,175 400	21,985 405	18,800 417			
7 M 46 DF	6,300	39,650 383	36,450 396	32,400 397	29,460 400	25,725 408	22,000 416			
8 M 46 DF	7,200	45,300 375	41,660 390	36,940 392	33,585 402	29,330 404	25,100 415			
9 M 46 DF	8,100	51,000 375	46,870 392	41,600 395	37,783 405	33,000 407	28,240 418			
Intake air te	emperature -	45°C – Dies	el operation							
6 M 46 DF	5,400	37,930 365	34,735 355	30,875 350	27,505 360	23,870 376	20,235 398			
7 M 46 DF	6,300	44,255 363	40,510 371	36,000 366	32,100 371	27,840 382	23,570 408			
8 M 46 DF	7,200	50,570 355	46,775 350	41,580 344	37,040 350	32,145 366	27,245 397			
9 M 46 DF	8,100	56,928 355	52,625 355	46,775 350	41,670 355	36,165 382	30,650 397			
Intake air te	emperature -	45°C – Gas	operation							
6 M 46 DF	5,400	32,530 408	29,905 421	26,583 424	24,170 424	21,105 429	18,050 442			
7 M 46 DF	6,300	38,065 406	34,995 420	31,105 421	28,285 424	24,700 432	21,120 441			
8 M 46 DF	7,200	433,488 397	39,995 413	35,462 415	32,242 426	28,157 428	24,100 440			
9 M 46 DF	8,100	48,960 397	44,995 415	39,940 419	36,272 429	31,680 431	27,110 443			

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2.4.2 Exhaust gas 965 kW/Cyl., 500rpm (MDO only) – preliminary

Tolerance: 5 % Relative humidity: 60 % Atmospheric pressure: 100 kPa (1 bar) Constant speed 500 rpm

Part	Atmospheric p	oressure:	100 kPa (1 bar) Constant speed 500 r			0 rpm					
Total Properties		Output		Output [%]							
Total Residence Total Resi	Fnaine	[LAA/]		[kg/h]							
Intake air temperature 25 °C - Diesel operation	Engine	[KVV]			[°	C]					
6 M 46 DF 5,790 42,325 38,713 34,410 30,655 26,605 22,550 7 M 46 DF 6,755 49,380 45,155 40,125 35,765 31,030 26,270 334 342 338 342 352 377 8 M 46 DF 7,720 56,485 52,135 46,340 41,285 35,830 30,365 9 M 46 DF 8,685 63,560 326 327 322 328 352 372 Intake air temperature 25 °C – Gas operation 8,685 38,514 35,200 31,300 28,450 24,845 21,245 386 398 7 M 46 DF 6,755 44,935 36,450 32,400 29,460 25,725 22,000 366 378 381 381 386 398 397 8 M 46 DF 7,720 51,400 41,660 36,940 33,585 29,330 25,100 39,88 390 401 1ntake air temperature 45 °C – Diesel operation 46,870 378 3			100	90	80	70	60	50			
6 M 46 DF 5,790 336 327 322 332 347 368 7 M 46 DF 6,755 49,380 45,155 40,125 35,765 31,030 26,270 8 M 46 DF 7,720 56,485 52,135 46,340 41,285 35,830 30,365 9 M 46 DF 8,685 63,560 58,650 52,135 46,443 40,310 34,160 9 M 46 DF 8,685 63,560 58,650 52,135 46,443 40,310 34,160 326 327 322 328 352 372 Intake air temperature 25 °C – Gas operation 6 M 46 DF 5,790 38,514 35,200 31,300 28,450 24,845 21,245 388 381 381 381 386 398 7 M 46 DF 6,755 364 377 378 381 389 397 8 M 46 DF 7,720 51,400 41,660 36,940 33,585 29,330 25,100	Intake air temperature 25 °C – Diesel operation										
7 M 46 DF 6,755 49,380 45,155 40,125 35,765 31,030 26,270 334 342 338 342 352 377 377 322 338 367 326 322 317 322 338 367 367 326 322 317 322 338 367 367 326 322 317 322 338 367 367 326 326 322 317 322 338 367 367 326 326 327 322 328 352 372 372 322 328 352 372 372 372 372 372 372 372 372 372 37	C N 1 1 C D F	F 700	42,325	38,713	34,410	30,655	26,605	22,550			
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7 M 46 DF 6,755 46,420	C N 4C DE	E 700	39,785	36,390	32,345	28,815	25,010	21,200			
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8 M 46 DF 7,720 53,100	7 M 46 DE	6 755									
8 M 46 DF 7,720 345 341 336 341 358 389 9 M 46 DF 8,685 59,750 55,130 48,010 43,660 37,890 32,110 345 345 347 341 348 373 394 Intake air temperature 45 °C – Gas operation 6 M 46 DF 5,790 36,025 33,090 29,420 26,745 23,355 19,970 404 404 404 409 422 7 M 46 DF 6,755 42,240 34,265 30,456 27,690 24,180 20,680 8 M 46 DF 7,720 48,315 39,160 34,725 31,570 27,570 23,595 8 M 46 DF 7,720 48,315 39,160 34,725 31,570 27,570 23,595 54,370 44,060 39,105 35,515 31,020 26,545	7 101 40 01	0,700									
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6 M 46 DF 5,790 388 401 404 404 409 422 7 M 46 DF 6,755 42,240 34,265 30,456 27,690 24,180 20,680 8 M 46 DF 7,720 48,315 39,160 34,725 31,570 27,570 23,595 379 395 397 408 410 422 54,370 44,060 39,105 35,515 31,020 26,545	intake air te	emperature			00.400	00.745	00.055	40.070			
7 M 46 DF 6,755 42,240 34,265 30,456 27,690 24,180 20,680 401 404 412 421 8 M 46 DF 7,720 48,315 39,160 34,725 31,570 27,570 23,595 379 395 397 408 410 422 54,370 44,060 39,105 35,515 31,020 26,545	6 M 46 DF	5,790		· ·		· ·					
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8 M 46 DF 7,720 48,315 39,160 34,725 31,570 27,570 23,595 395 397 408 410 422 54,370 44,060 39,105 35,515 31,020 26,545	7 M 46 DF	6,755						1			
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5/ 370	8 M 46 DF	7,720				· ·					
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9 M 46 DF 8,685 37,9 397 401 411 413 425	9 IVI 46 DF	8,685									

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2.4.3 Exhaust gas 965 kW/Cyl., 514 rpm (MDO only) – preliminary

Tolerance: 5 % Relative humidity: 60 % Atmospheric pressure: 100 kPa (1 bar) Constant speed 514 rpm

	oressure:	100 kPa (1 ba	лі <i>ј</i>	COI	istant speed	J1.	4 rpm			
	Output			Outp	ut [%]					
F	[1] [1]	[kg/h]								
Engine	[kW]			[°	C]					
		100	90	80	70	60	50			
Intake air te	emperature	25 °C – Dies	el operation							
C M 40 DE	Г 700	41,474	37,938	33,720	30,040	26,075	22,100			
6 M 46 DF	5,790	336	327	322	332	347	368			
7 M 46 DF	6,755	48,389	44,250	39,320	35,050	30,410	25,745			
7 IVI +0 DI	0,700	334	342	338	342	352	377			
8 M 46 DF	7,720	55,360	51,090	45,415	40,460	35,115	29,760			
0 111 10 21	. ,. =0	326	322	317	322	338	367			
9 M 46 DF	8,685	62,295	57,480	51,090	45,515	39,505	33,480			
		326	327	322	328	352	372			
Intake air te	emperature	25 °C – Gas		00.075	07.000	04.050	00.000			
6 M 46 DF	5,790	37,742	34,495	30,675	27,880 381	24,350	20,820			
		366	378	381		386	398			
7 M 46 DF	6,755	44,035 364	35,720 377	31,750 378	28,870 381	25,210 389	21,560 397			
		50,380	40,825	36,200	32,915	28,745	24,600			
8 M 46 DF	7,720	358	373	375	385	387	398			
0.14.40.05	0.005	56,688	45,930	40,770	37,030	32,340	27,675			
9 M 46 DF	8,685	358	375	378	388	390	401			
Intake air te	emperature	45 °C – Dies	el operation							
6 M 46 DF	5,790	38,985	35,662	31,700	28,240	24,510	20,775			
0 IVI 40 DF	3,790	358	349	343	354	370	393			
7 M 46 DF	6,755	45,485	41,595	36,960	32,950	28,585	24,200			
7 101 70 01	0,700	354	365	358	365	373	400			
8 M 46 DF	7,720	52,040	48,025	42,690	38,030	33,010	27,975			
		348	343	338	341	358	389			
9 M 46 DF	8,685	58,560	54,030	48,025	42,785	37,135	31,470			
Intoles sints		348	347	341	348	373	394			
intake air te	emperature	45 °C – Gas		00.005	00.010	00.000	10.570			
6 M 46 DF	5,790	35,480 388	32,425 401	28,835 404	26,210 403	22,890 409	19,570 422			
		41,395	33,580	29,845	27,140	23,700	20,270			
7 M 46 DF	6,755	386	400	401	403	412	421			
		47,360	38,375	34,030	30,940	27,020	23,125			
8 M 46 DF	7,720	379	395	397	408	410	422			
0 14 40 DE	0.005	53,290	43,175	38,325	34,810	30,400	26,015			
9 M 46 DF	8,685	379	397	401	411	413	425			

GENERAL DATA AND OUTPUTS

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2.4.4 Nitrogen oxide emissions (NO_x-values)

 NO_x -limit values according to IMO II: 10.54 g/kWh (n=500 rpm)

Main engine: DE-drive acc. to cycle E2: 10.3 g/kWh Auxiliary genset acc. cycle D2: 10.3 g/kWh

 NO_{y} -limit values according to IMO III: 2.60 g/kWh (n=500 rpm)

Gas mode (cycle E2 and D2): 2.60 g/kWh

2.4.5 Engine International Air Pollution Prevention Certificate

The MARPOL Diplomatic Conference has agreed about a limitation of NO_x emissions, referred to as Annex VI to MARPOL 73/78.

When testing the engine for NO_x emissions, the reference fuel is marine diesel oil (distillate) and the test is performed according to ISO 8178 test cycles:

	Test cycle type E2					Test	cycle typ	e D2	
Speed	100 %	100 %	100 %	100 %	100 %	100 %	100 %	100 %	100 %
Power	100 %	75 %	50 %	25 %	100 %	75 %	50 %	25 %	10 %
Weighting factor	0.2	0.5	0.15	0.15	0.05	0.25	0.3	0.3	0.1

Subsequently, the NO_x value is calculated using different weighting factors for different loads that have been corrected to ISO 8178 conditions.

A NO_x emission evidence will be issued for each engine showing that the engine complies with the regulation. The evidence will come as EAPP (Engine Air Pollution Prevention) Statement of Compliance, EAPP Document of Compliance or EIAPP (Engine International Air Pollution Prevention) Certificate according to the authorization by the flag state and related technical file. For the most part on basis of an EAPP Statement of Compliance or an EAPP Document of Compliance an EIAPP certificate can be applied for.

According to the IMO regulations, a technical file shall be provided for each engine. This technical file contains information about the components affecting NO_X emissions, and each critical component is marked with a special IMO number. Such critical components are piston, cylinder head, injection nozzle (element), camshaft section, fuel injection pump, turbocharger and charge air cooler. The allowable settings and parameters for running the engine are also specified in the technical file.

The marked components can be easily identified on-board of the ship by the surveyor and thus an IAPP (International Air Pollution Prevention) certificate for the ship can be issued on basis of the EIAPP certificate and the on-board inspection.

GENERAL DATA AND OUTPUTS

2.5 Engine dimensions and weight – preliminary

Turbocharger at free end

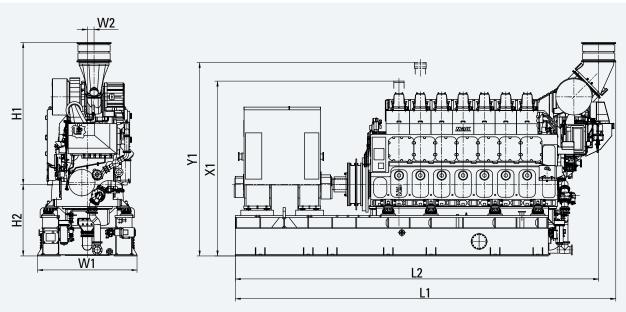


Fig. 2-1 Turbocharger at free end

Туре	Dimensions [mm]								
	L1	L2	H1	H2	W1	W2	[t]		
6 M 46 DF	12,202	11,651	4,358	2,444	3,400	215	178.0		
7 M 46 DF	12,999	12,414	4,849	2,444	3,400	232	195.0		
8 M 46 DF	13,729	13,144	4,849	2,444	3,400	232	210.0		
9 M 46 DF	14,459	13,874	4,849	2,444	3,400	232	240.0		

^{*)} Depending on generator weight

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System connecting points – preliminary 2.6

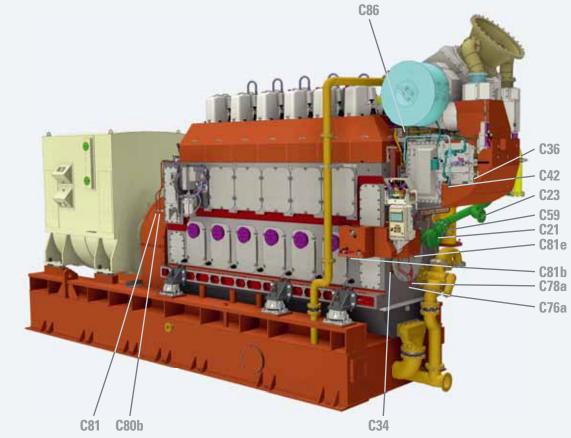


Fig. 2-2 Connecting points at the engine -1

C21	Fresh water pump HT, inlet	C78a	Pilot fuel, outlet
C23	Fresh water pump HT, outlet	C80b	Drip fuel connection (cut off pump)
C34	Drain, condensate separator	C81	Drip fuel connection
C36	Drain, turbocharger washing	C81b	Drip fuel connection (filter pan)
C42	Turbine cleaning connection	C81e	Drip fuel connection, pilot fuel
C59	Lube oil, inlet	C86	Connection starting air
C76a	Pilot fuel, inlet		

GENERAL DATA AND OUTPUTS

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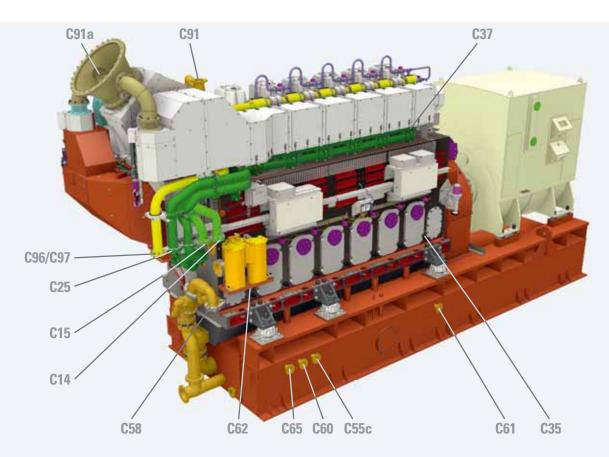


Fig. 2-3 Connecting points at the engine -2

C14	Charge air cooler LT, inlet	C61	Separator connection, delivery side
C15	Charge air cooler LT, outlet	C62	Drip oil, pan duplex filter
C25	Cooling water, engine outlet	C65	Lube oil filling socket
C35	Charge air duct, drain	C91	Crankcase ventilation to stack
C37	Vent	C91a	Exhaust gas outlet
C55c	Connection flushing pipe automatic filter	C96	Gas inlet
C58	Force pump, delivery side	C97	Flushing connection gas pipe (inert gas)
C60	Separator connection, suction side		

3.1 Restrictions for low load operation

3.1.1 Load restrictions in diesel mode

The engine can be started, stopped and run on heavy fuel oil under all operating conditions. The HFO system of the engine remains in operation and keeps the HFO at injection viscosity. The temperature of the engine injection system is maintained by circulating hot HFO and heat losses are compensated.

The lube oil treatment system (lube oil separator) remains in operation, the lube oil is separated continuously. The operating temperature of the engine cooling water is maintained by the cooling water preheater. Below 25 % output heavy fuel operation is neither efficient nor economical.

A change-over to diesel oil is recommended to avoid disadvantages as e.g. increased wear and tear, contamination of the air and exhaust gas systems and increased contamination of lube oil.

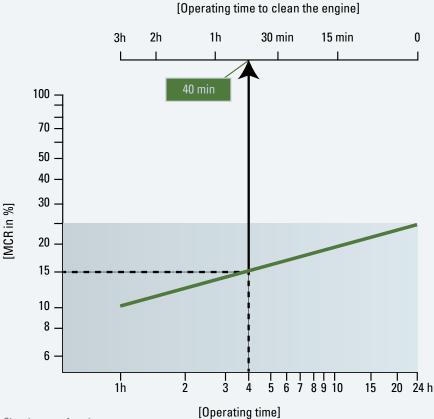


Fig. 3-1 Cleaning run of engine

3.1.2 Load restrictions in gas mode

A gas operation above 100% load is prohibited. A gas operation below 15 % (965 kW/cyl.) or 10 % (900 kW/cyl.) load is not possible or limited for a certain time. The ability to start the engine in gas operation is optional available.

A direct fuel change over from HFO operation to gas operation is prohibited. The engine needs to run a certain time with MDO before change over to gas operation.

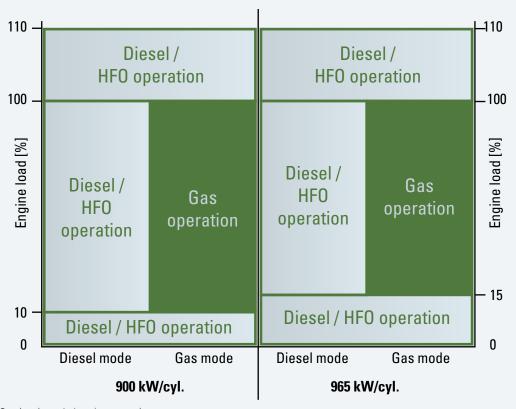


Fig. 3-2 Load restrictions in gas mode

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3.2 Emergency operation without turbocharger

Emergency operation is permissible with MDO only up to approx. 15% of the MCR.

3.3 Operation in inclined position

Inclination angles of ships at which engine running must be possible:

Rotation X-axis:

Heel to each side: 15° Rolling to each side: 22.5°

Rotation Y-axis:

Trim by head and stern: 5° Pitching: $\pm 7.5^{\circ}$

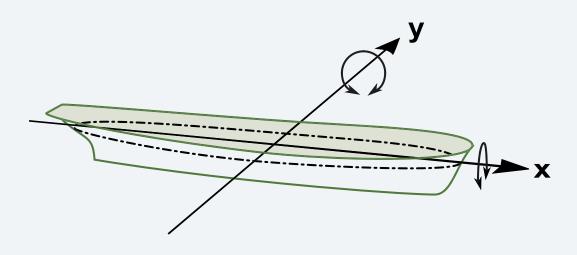
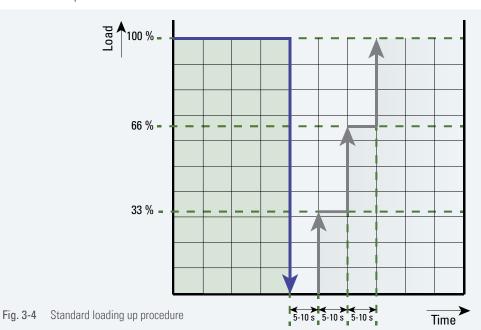


Fig. 3-3 Rotation axis

3.4 Load application and recovery behaviour

Our standard loading up procedure for M 46 DF engines is to achieve recovery behaviour in accordance with class requirements.

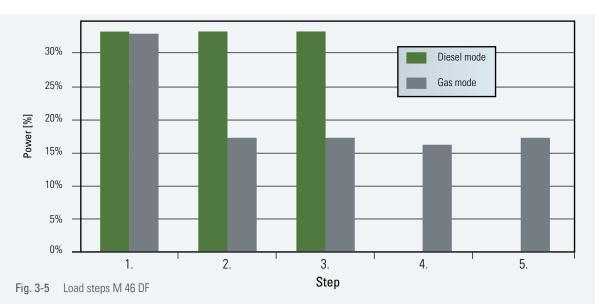


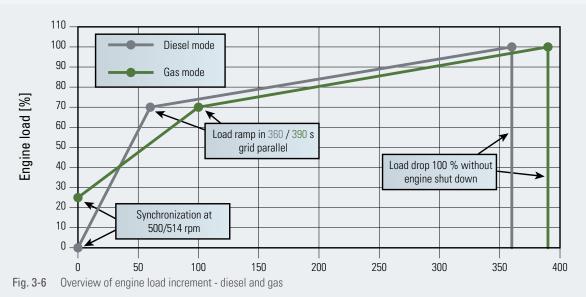
		Power [%]	
Steps	1.	2.	3.
Diesel mode	33.3 %	33.3 %	33.3 %

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	Power [%]						
Steps	1.	2.	3.	4.	5.		
Diesel mode	33.3 %	33.3 %	33.3 %				
Gas mode	33.0 %	17.0 %	17.0 %	16.0 %	17 0 %		





Remarks:

Instant loading with recovery time in 5 seconds, ToI.: \pm 5 seconds, engine warmed up in operating conditions

Minimum operating time 10 minutes

Lube oil > 50 °C

Coolant > 65 °C



3.5 Fuel changeover and recovery behaviour

a) Changeover from gas to diesel operation:

- Changeover from gas to diesel fuel operation is done within approx. 1 second at any load, if required due to emergency switch over. The normal switchover takes approx. 300 seconds.
- Changeover can be started manually by operator or automatically by MACS, if the gas operation conditions are not given anymore (e.g. load window for gas operation has been left).
 - Main liquid fuel injection activated
 - Gaseous fuel slowly cut back / liquid fuel amount rises
 - FCT: Valve timing adjusts depending on running condition (e.g. load)
 - Air fuel ratio control is shut-off (Blow-Off and Waste Gate)
 - Pilot injection is still active

b) Changeover from diesel to gas operation:

- Changeover from diesel to gas fuel operation is possible in the load range between 15% and 100% power.
- If gas mode is activated, the load is constant in the correct range and all systems are running, the engine control will change over to gas operation:
 - Start air fuel ratio control with exhaust Waste Gate and Blow-Off
 - Change valve timing over to gas operation depending on running conditions
 - Start gas supply and raise gas amount, if gas pressure is sufficient
 - Main liquid fuel injection cuts back and switches off, if minimum fuel rack position is reached
- The procedure will take approx. 2 minutes, which depends on gas supply system and self check procedures.
- If the procedure is completed, power ramp up to 100% power or instant loading is possible.

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3.6 Derating

In case of a fuel gas methane number lower than 80, the power output has to be redetermined in gas operation.

For an alternative derating curve please consult Caterpillar Motoren in advance.

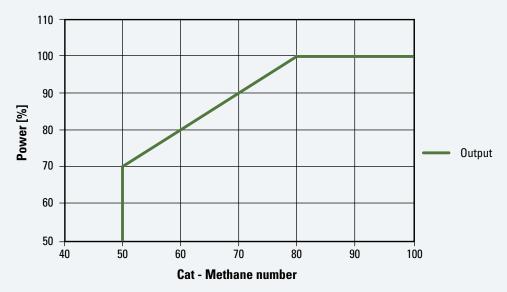


Fig. 3-7 Power as function of methane number

TECHNICAL DATA

4.1 Diesel, mechanical

4.1.1 Output 900 kW/Cyl. in HFO, MDO and gas operation

Output 900 kW/Cyl. (HFO,	MDO and gas)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Performance data					
Maximum continuous rating acc. ISO 3046/1	[kW]	5,400	6,300	7,200	8,100
Speed	[rpm]	500/514	500/514	500/514	500/514
Minimum speed	[rpm]	300	300	300	300
Brake mean effective presure	[bar]	21.3/20.7	21.3/20.7	21.3/20.7	21.3/20.7
Charge air pressure	[bar]	3.55	3.55	3.55	3.55
Firing pressure (max. allowed, tolerance +/- 3%)	[bar]	190	190	190	190
Combustion air demand (ta=20°C)	[m³/h]	32,050	37,380	42,720	48,060
Max. load acceptance	[kW/s]	33	39	45	50
Specific fuel oil consumption diesel/gas					
$n = const^{1}$ 100 %	[g/kWh] [kJ/kWh]	186/7,400	186/7,400	186/7,400	186/7,400
85 %	[g/kWh] [kJ/kWh]	185/7,524	185/,7524	185/7,524	185/7,524
75 %	[g/kWh] [kJ/kWh]	187/7,457	187/7,457	187/7,457	187/7,457
50 %	[g/kWh] [kJ/kWh]	192/7,929	192/7,929	192/7,929	192/7,929
Lube oil consumption 2)	[g/kWh]	0.6	0.6	0.6	0.6
NO _x -emission (diesel) 6)	[g/kWh]	10.3	10.3	10.3	10.3
NO _x -emission (gas) ⁶⁾	[g/kWh]	2.6	2.6	2.6	2.6
Methane slip, sp. pilot oil injection					
100 %	[% kJ/kWh]	2.0/72	2.0/72	2.0/72	2.0/72
50 %	[% kJ/kWh]	2.1/96	2.1/96	2.1/96	2.1/96
15 %	[% kJ/kWh]	6.9/272	6.9/272	6.9/272	6.9/272
CO ₂ 100% (diesel/gas)	[%]	5.4/4.5	5.4/4.5	5.4/4.5	5.4/4.5
Turbocharger type		ABB TPL71	ABB TPL76	ABB TPL76	ABB TPL76
Fuel					
Engine driven booster pump	[m³/h] [bar]	-/-	-/-	-/-	-/-
Stand-by booster pump	[m³/h] [bar]	4.2/10	4.9/10	5.6/10	6.3/10
Mesh size MDO fine filter	[mm]	0.025	0.025	0.025	0.025
Mesh size HFO automatic filter	[mm]	0.010	0.010	0.010	0.010
Mesh size HFO fine filter	[mm]	0.034	0.034	0.034	0.034

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Output 900 kW/Cyl. (HFO, MDO a	and gas)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Lube oil					
Engine driven pump	[m³/h] [bar]	146/10	146/10	203/10	203/10
Independent pump	[m³/h] [bar]	120/10	140/10	160/10	180/10
Working pressure on engine inlet	[bar]	4 - 5	4 - 5	4 - 5	4 - 5
Engine driven suction pump	[m³/h] [bar]	-/-	-/-	-/-	-/-
Independent suction pump	[m³/h] [bar]	175/3	175/3	240/3	240/3
Priming pump pressure / suck pump	[m³/h] [bar]	16/5	16/5	20/5	20/5
Sump tank content / dry sump content	[m³]	8.4	9.8	11.2	12.6
Temperature at engine inlet	[°C]	60 - 65	60 - 65	60 - 65	60 - 65
Temperature controller NB	[mm]	125	125	150	150
Double filter NB	[mm]	150	150	150	150
Mesh size double filter	[mm]	0.08	0.08	0.08	0.08
Mesh size automatic filter	[mm]	0.03	0.03	0.03	0.03
Fresh water cooling					
Engine content	[m³]	0.6	0.7	0.8	0.9
Pressure at engine inlet min/max	[bar]	2.5/6.0	2.5/6.0	2.5/6.0	2.5/6.0
Header tank capacity	[m³]	0.6	0.6	0.6	0.6
Temperature at engine outlet	[°C]	80 - 90	80 - 90	80 - 90	80 - 90
Two circuit system					
Engine driven pump HT	[m³/h] [bar]	100/4.5	100/4.5	120/4.3	120/4.3
Independent pump HT	[m³/h] [bar]	100/4.5	110/4.5	120/4.5	130/4.5
HT-controller NB	[mm]	125	125	150	150
Water demand LT-charge air cooler	[m³/h]	80	80	100	100
Temperature LT-charge air cooler inlet	[°C]	38	38	38	38
Heat dissipation *)					
Specific jacket water heat	[kJ/kWh]	496	496	496	496
Specific lube oil heat	[kJ/kWh]	500	500	500	500
Lube oil cooler	[kW]	750	875	1,000	1,120
Jacket water	[kW]	745	870	995	1,115
Charge air cooler 3)	[kW]	_	_	_	_
Charge air cooler (HT-stage) 3)	[kW]	1,770	2,065	2,360	2,655
Charge air cooler (LT-stage) 3) (HT-stage before engine)	[kW]	500	585	665	750
Heat radiation engine	[kW]	255	300	340	380

 $^{^{*)}}$ NOTE: Tolerance for heat and exhaust flow +/- 10 %, tolerance of +10 % for rating coolers

Output 900 kW/Cyl. (HFO, MDC) and gas)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Exhaust gas					
Silencer / spark arrestor NB	[mm]	900	1,000	1,000	1,000
Pipe diameter NB after turbine	[mm]	900	1,000	1,000	1,000
Exhaust gas temperature after turbine (intake air 25 °C, diesel) 5)	[°C)	345	343	335	335
Exhaust gas mass flow (intake air 25 °C, diesel) 5)	[kg/h]	39,510	46,100	52,675	59,300
Exhaust gas temperature after turbine (intake air 25 °C, gas) 5)	[°C]	385	383	375	375
Exhaust gas mass flow (intake air 25 °C, gas) 5)	[kg/h]	33,885	39,650	45,300	51,000
Maximum exhaust gas pressure drop	[bar]	0.03	0.03	0.03	0.03
Starting air					
Maximum starting air pressure	[bar]	30	30	30	30
Minimum starting air pressure	[bar]	14	14	14	14
Air consumption per start 4)	[Nm³]	2.6	2.7	3.2	3.3
Air consumption per slow turn maneuver 4)	[Nm³]	5.2	5.4	6.4	6.6
Max. allowed crankcase pressure, ND ventilation pipe	[mmWs/mm]	15/150	15/150	15/150	15/150

1) Reference conditions: LCV = 42,700 kJ/kg, ambient temperature 25 °C, charge air coolant temperature 25 °C, tolerance 5 %, for engine driven oil pump +1% at 100%, 1.2% at 85%, 1.3% at 75%, 2% at 50%, 4% at 25%, for engine driven cooling water pump +0.4% at 100%, 0.47% at 85%, 0.53% at 75%, 0.8% at 50%, 1.6% at 25%, in propeller operation for engine driven oil pump +1% at 100%, 1.1% at 85%, 1.2% at 75%, 1.4% at 50%, 2% at 25%, for engine driven cooling water pump +0.4% at 100/85/75/50/25%, additions to fuel consumption must be considered before tolerance is taken into account. / 2) Standard value, tolerance ± 0.3 g/kWh, related on full load / 3) Charge air heat based on 45 °C ambient temperature / 4) Preheated engine / 5) Tolerance 10 %, rel. humidity 60 % / 6) Marpol 73/78, Annex VI, cycle E2, D

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4.1.2 Output 965 kW/Cyl. in MDO and gas operation only – preliminary

4.1.2.1 Output 965 kW/Cyl. at 500 rpm – preliminary

Output 965 kW/Cyl., 500 rpm (N	IDO and gas only)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Performance data					
Maximum continuous rating acc. ISO 3046/1	[kW]	5,790	6,755	7,720	8,685
Speed	[rpm]	500	500	500	500
Minimum speed	[rpm]	300	300	300	300
Brake mean effective presure	[bar]	22.8	22.8	22.8	22.8
Charge air pressure	[bar]	4.0	4.0	4.0	4.0
Firing pressure (max. allowed, tolerance +/- 3%)	[bar]	190	190	190	190
Combustion air demand (ta=20°C)	[m³/h]	34,240	39,950	45,700	51,425
Max. load acceptance	[kW/s]	33	39	45	50
Specific fuel oil consumption diesel/gas					
$n = const^{-1}$ 100 %	[g/kWh] [kJ/kWh]	185/7,350	185/7,350	185/7,350	185/7,350
85 %	[g/kWh] [kJ/kWh]	183/7,445	183/7,445	183/7,445	183/7,445
75 %	[g/kWh] [kJ/kWh]	184/7,490	184/7,490	184/7,490	184/7,490
50 %	[g/kWh] [kJ/kWh]	188/7,740	188/7,740	188/7,740	188/7,740
Lube oil consumption 2)	[g/kWh]	0.6	0.6	0.6	0.6
NO _x -emission (diesel) ⁶⁾	[g/kWh]	10.3	10.3	10.3	10.3
NO _x -emission (gas) ⁶⁾	[g/kWh]	2.6	2.6	2.6	2.6
Methane slip, sp. pilot oil injection					
100 %	[% kJ/kWh]	2.0/72	2.0/72	2.0/72	2.0/72
50 %	[% kJ/kWh]	2.1/96	2.1/96	2.1/96	2.1/96
15 %	[% kJ/kWh]	6.9/272	6.9/272	6.9/272	6.9/272
CO ₂ 100% (diesel/gas)	[%]	5.4/4.5	5.4/4.5	5.4/4.5	5.4/4.5
Turbocharger type		ABB TPL71	ABB TPL76	ABB TPL76	ABB TPL76
Fuel					
Engine driven booster pump	[m³/h] [bar]	-/-	-/-	-/-	_/_
Stand-by booster pump	[m³/h] [bar]	4.2/10	4.9/10	5.6/10	6.3/10
Mesh size MDO fine filter	[mm]	0.025	0.025	0.025	0.025

Output 965 kW/Cyl., 500 rpm (MDO ai	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF	
Lube oil					
Engine driven pump	[m³/h] [bar]	146/10	146/10	203/10	203/10
Independent pump	[m³/h] [bar]	120/10	140/10	160/10	180/10
Working pressure on engine inlet	[bar]	4 - 5	4 - 5	4 - 5	4 - 5
Engine driven suction pump	[m³/h] [bar]	-/-	-/-	-/-	-/-
Independent suction pump	[m³/h] [bar]	175/3	175/3	240/3	240/3
Priming pump pressure / suck pump	[m³/h] [bar]	16/5	16/5	20/5	20/5
Sump tank content / dry sump content	[m³]	8.4	9.8	11.2	12.6
Temperature at engine inlet	[°C]	60 - 65	60 - 65	60 - 65	60 - 65
Temperature controller NB	[mm]	125	125	150	150
Double filter NB	[mm]	150	150	150	150
Mesh size double filter	[mm]	0.08	0.08	0.08	0.08
Mesh size automatic filter	[mm]	0.03	0.03	0.03	0.03
Fresh water cooling					
Engine content	[m³]	0.6	0.7	0.8	0.9
Pressure at engine inlet min/max	[bar]	2.5/6.0	2.5/6.0	2.5/6.0	2.5/6.0
Header tank capacity	[m³]	0.6	0.6	0.6	0.6
Temperature at engine outlet	[°C]	80 - 90	80 - 90	80 - 90	80 - 90
Two circuit system					
Engine driven pump HT	[m³/h] [bar]	100/4.5	100/4.5	120/4.3	120/4.3
Independent pump HT	[m³/h] [bar]	100/4.5	110/4.5	120/4.5	130/4.5
HT-controller NB	[mm]	125	125	150	150
Water demand LT-charge air cooler	[m³/h]	80	80	100	100
Temperature LT-charge air cooler inlet	[°C]	38	38	38	38
Heat dissipation *)					
Specific jacket water heat	[kJ/kWh]	480	480	480	480
Specific lube oil heat	[kJ/kWh]	482	482	482	482
Lube oil cooler	[kW]	775	905	1,035	1,160
Jacket water	[kW]	775	900	1,030	1,155
Charge air cooler 3)	[kW]	_	_	_	_
Charge air cooler (HT-stage) 3)	[kW]	2,000	2,330	2,665	2,995
Charge air cooler (LT-stage) 3) (HT-stage before engine)	[kW]	530	615	705	790
Heat radiation engine	[kW]	270	320	365	410

 $^{^{*)}}$ NOTE: Tolerance for heat and exhaust flow +/- 10 %, tolerance of +10 % for rating coolers

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Output 965 kW/Cyl., 500 rpm (MDO	and aga anly)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
<u> </u>	anu yas omy	0 IVI 40 DF	/ IVI 40 DF	0 IVI 40 DF	9 IVI 40 DF
Exhaust gas	ı	ı	ı	ı	ı
Silencer / spark arrestor NB	[mm]	900	1,000	1,000	1,000
Pipe diameter NB after turbine	[mm]	900	1,000	1,000	1,000
Exhaust gas temperature after turbine (intake air 25 °C, diesel) 5)	[°C)	336	334	326	326
Exhaust gas mass flow (intake air 25 °C, diesel) 5)	[kg/h]	42,325	49,380	56,485	63,560
Exhaust gas temperature after turbine (intake air 25 °C, gas) 5)	[°C]	366	364	358	358
Exhaust gas mass flow (intake air 25 °C, gas) 5)	[kg/h]	38,514	44,935	51,400	57,840
Maximum exhaust gas pressure drop	[bar]	0.03	0.03	0.03	0.03
Starting air					
Maximum starting air pressure	[bar]	30	30	30	30
Minimum starting air pressure	[bar]	14	14	14	14
Air consumption per start 4)	[Nm³]	2.6	2.7	3.2	3.3
Air consumption per slow turn maneuver 4)	[Nm³]	5.2	5.4	6.4	6.6
Max. allowed crankcase pressure, ND ventilation pipe	[mmWs/mm]	15/150	15/150	15/150	15/150

1) Reference conditions: LCV = 42,700 kJ/kg, ambient temperature 25 °C, charge air coolant temperature 25 °C, tolerance 5 %, for engine driven oil pump +1% at 100%, 1.18% at 85%, 1.33% at 75%, 2% at 50%, 4% at 25%, for engine driven cooling water pump +0.4% at 100%, 0.47% at 85%, 0.53% at 75%, 0.8% at 50%, 1.6% at 25%, additions to fuel consumption must be considered before tolerance is taken into account. / 2) Standard value, tolerance \pm 0.3 g/kWh, related on full load / 3) Charge air heat based on 45 °C ambient temperature / 4) Preheated engine / 5) Tolerance 10 %, rel. humidity 60 % / 6) Marpol 73/78, Annex VI, cycle E2, D

4.1.2.2 Output 965 kW/Cyl. at 514 rpm – preliminary

Output 965 kW/Cyl., 500 rpm (N	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF	
Performance data					
Maximum continuous rating acc. ISO 3046/1	[kW]	5,790	6,755	7,720	8,685
Speed	[rpm]	514	514	514	514
Minimum speed	[rpm]	300	300	300	300
Brake mean effective presure	[bar]	22.2	22.2	22.2	22.2
Charge air pressure	[bar]	3.83	3.83	3.83	3.83
Firing pressure (max. allowed, tolerance +/- 3%)	[bar]	190	190	190	190
Combustion air demand (ta=20°C)	[m³/h]	33,555	39,150	44,790	50,400
Max. load acceptance	[kW/s]	33	39	45	50
Specific fuel oil consumption diesel/gas					
n = const 1) 100 %	[g/kWh] [kJ/kWh]	186/7,350	186/7,350	186/7,350	186/7,350
85 %	[g/kWh] [kJ/kWh]	184/7,460	184/7,460	184/7,460	184/7,460
75 %	[g/kWh] [kJ/kWh]	185/7,490	185/7,490	185/7,490	185/7,490
50 %	[g/kWh] [kJ/kWh]	189/7,740	189/7,740	189/7,740	189/7,740
Lube oil consumption 2)	[g/kWh]	0.6	0.6	0.6	0.6
NO _x -emission (diesel) ⁶⁾	[g/kWh]	10.3	10.3	10.3	10.3
NO _x -emission (gas) ⁶⁾	[g/kWh]	2.6	2.6	2.6	2.6
Methane slip, sp. pilot oil injection					
100 %	[% kJ/kWh]	2.0/72	2.0/72	2.0/72	2.0/72
50 %	[% kJ/kWh]	2.1/96	2.1/96	2.1/96	2.1/96
15 %	[% kJ/kWh]	6.9/272	6.9/272	6.9/272	6.9/272
CO ₂ 100% (diesel/gas)	[%]	5.4/4.5	5.4/4.5	5.4/4.5	5.4/4.5
Turbocharger type		ABB TPL71	ABB TPL76	ABB TPL76	ABB TPL76
Fuel					
Engine driven booster pump	[m³/h] [bar]	-/-	-/-	-/-	-/-
Stand-by booster pump	[m³/h] [bar]	4.2/10	4.9/10	5.6/10	6.3/10
Mesh size MDO fine filter	[mm]	0.025	0.025	0.025	0.025

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Output 965 kW/Cyl., 500 rpm (MDO a	nd gas only)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Lube oil					
Engine driven pump	[m³/h] [bar]	146/10	146/10	203/10	203/10
Independent pump	[m³/h] [bar]	120/10	140/10	160/10	180/10
Working pressure on engine inlet	[bar]	4 - 5	4 - 5	4 - 5	4 - 5
Engine driven suction pump	[m³/h] [bar]	-/-	-/-	-/-	-/-
Independent suction pump	[m³/h] [bar]	175/3	175/3	240/3	240/3
Priming pump pressure / suck pump	[m³/h] [bar]	16/5	16/5	20/5	20/5
Sump tank content / dry sump content	[m³]	8.4	9.8	11.2	12.6
Temperature at engine inlet	[°C]	60 - 65	60 - 65	60 - 65	60 - 65
Temperature controller NB	[mm]	125	125	150	150
Double filter NB	[mm]	150	150	150	150
Mesh size double filter	[mm]	0.08	0.08	0.08	0.08
Mesh size automatic filter	[mm]	0.03	0.03	0.03	0.03
Fresh water cooling					
Engine content	[m³]	0.6	0.7	0.8	0.9
Pressure at engine inlet min/max	[bar]	2.5/6.0	2.5/6.0	2.5/6.0	2.5/6.0
Header tank capacity	[m³]	0.6	0.6	0.6	0.6
Temperature at engine outlet	[°C]	80 - 90	80 - 90	80 - 90	80 - 90
Two circuit system					
Engine driven pump HT	[m³/h] [bar]	100/4.5	100/4.5	120/4.3	120/4.3
Independent pump HT	[m³/h] [bar]	100/4.5	110/4.5	120/4.5	130/4.5
HT-controller NB	[mm]	125	125	150	150
Water demand LT-charge air cooler	[m³/h]	80	80	100	100
Temperature LT-charge air cooler inlet	[°C]	38	38	38	38
Heat dissipation *)					
Specific jacket water heat	[kJ/kWh]	480	480	480	480
Specific lube oil heat	[kJ/kWh]	482	482	482	482
Lube oil cooler	[kW]	775	905	1,035	1,160
Jacket water	[kW]	775	900	1,030	1,155
Charge air cooler 3)	[kW]	_	_	_	_
Charge air cooler (HT-stage) 3)	[kW]	2,000	2,330	2,665	2,995
Charge air cooler (LT-stage) 3) (HT-stage before engine)	[kW]	530	615	705	790
Heat radiation engine	[kW]	270	320	365	410

 $^{^{*)}}$ NOTE: Tolerance for heat and exhaust flow +/- 10 %, tolerance of +10 % for rating coolers

Output 965 kW/Cyl., 500 rpm (MDO	and gas only)	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Exhaust gas					
Silencer / spark arrestor NB	[mm]	900	1,000	1,000	1,000
Pipe diameter NB after turbine	[mm]	900	1,000	1,000	1,000
Exhaust gas temperature after turbine (intake air 25 °C, diesel) 5)	[°C)	336	334	326	326
Exhaust gas mass flow (intake air 25 °C, diesel) $^{5)}$	[kg/h]	41,474	48,389	55,360	62,295
Exhaust gas temperature after turbine (intake air 25 °C, gas) 5)	[°C]	366	364	358	358
Exhaust gas mass flow (intake air 25 °C, gas) ⁵⁾	[kg/h]	37,742	44,035	50,380	56,688
Maximum exhaust gas pressure drop	[bar]	0.03	0.03	0.03	0.03
Starting air					
Maximum starting air pressure	[bar]	30	30	30	30
Minimum starting air pressure	[bar]	14	14	14	14
Air consumption per start 4)	[Nm³]	2.6	2.7	3.2	3.3
Air consumption per slow turn maneuver 4)	[Nm³]	5.2	5.4	6.4	6.6
Max. allowed crankcase pressure, ND ventilation pipe	[mmWs/mm]	15/150	15/150	15/150	15/150

1) Reference conditions: LCV = 42,700 kJ/kg, ambient temperature 25 °C, charge air coolant temperature 25 °C, tolerance 5 %, for engine driven oil pump +1% at 100%, 1.18% at 85%, 1.33% at 75%, 2% at 50%, 4% at 25%, for engine driven cooling water pump +0.4% at 100%, 0.47% at 85%, 0.53% at 75%, 0.8% at 50%, 1.6% at 25%, additions to fuel consumption must be considered before tolerance is taken into account. / 2) Standard value, tolerance ± 0.3 g/kWh, related on full load / 3) Charge air heat based on 45 °C ambient temperature / 4) Preheated engine / 5) Tolerance 10 %, rel. humidity 60 % / 6) Marpol 73/78, Annex VI, cycle E2, D

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5.1 MGO / MDO operation

General

MaK diesel engines are designed to burn a wide variety of fuels.

See the information on fuel requirements in section MDO / MGO and HFO operation or consult the Caterpillar Motoren technical product support.

For proper operation of MaK engines the minimum Caterpillar Motoren requirements for storage, treatment and supply systems have to be observed, as shown in the following sections.

5.1.1 Acceptable MGO / MDO characteristics

Two fuel product groups are permitted for MaK engines:

Pure distillates: Gas oil, marine gas oil, diesel fuel

Distillate/mixed fuels: Marine gas oil (MGO), marine diesel oil (MDO)

The difference between distillate/mixed fuels and pure distillates are higher density, sulfur content and viscosity.

Marine distillate fuels

Parameter	Unit	Limit	DMX	DMA	DMZ	DMB
Viscosity at 40 °C	[mm²/s]	max	5.5	6.0	6.0	11.0
Viscosity at 40 °C	[mm²/s]	min	1.4	2.0	3.0	2.0
Micro Carbon residue at 10 % residue	[% m/m]	max	0.3	0.0	0.3	_
Density at 15 °C	[kg/m³]	max	_	890	890	900
Micro Carbon residue	[% m/m]	max	_	_	_	0.3
Sulfur a)	[% m/m]	max	1.0	1.5	1.5	2.0
Water	[% V/V]	max	_	_	_	0.3 b)
Total sediment by hot filtration	[% m/m]	max	_	_	_	0.1 b)
Ash	[% m/m]	max	0.01	0.01	0.01	0.01
Flash point	[°C]	min	43	60	60	60
Pour point, summer	[°C]	max	_	0	0	6
Pour point, winter	[°C]	max	_	-6	-6	0
Cloud point	[°C]	max	-16	_	_	_
Calculated Cetane Index		min	45	40	40	35
Acid number	[mgKOH/g]	max	0.5	0.5	0.5	0.5
Oxidation stability	[g/m³]	max	25	25	25	25 ^{c)}
Lubricity, corrected wear scar diameter (wsd 1.4 at 60 °C) d)	[µm]	max	520	520	520	520 ^{c)}
Hydrogen sulfide ^{e)}	[mg/kg]	max	2.0	2.0	2.0	2.0
Appearance			cl	b), c)		

a) A Sulphur limit of 1.00 % m/m applies in the Emission Control Areas designated by the International Maritime Organization. As there may be local variations, the purchaser shall define the maximum Sulphur content according to the relevant statutory requirements, notwithstanding the limits given in this table. / b) If the sample is not clear and bright, total sediment by hot filtration and water test shall be required. / c) Oxidation stability and lubricity tests are not applicable if the sample is not clear and bright. / d) Applicable if Sulphur is less than 0.050% m/m. / e) Effective only from 1 July 2012. / f) If the sample is dyed and not transparent, water test shall be required. The water content shall not exceed 200 mg/kg (0.02% m/m).

5.1.2 Internal fuel oil system

General

The fuel injectors are utilized to deliver the correct amount of fuel to the cylinders precisely at the moment it is needed. The diesel fuel supply system must ensure a permanent and clean supply of diesel fuel to the engine internal fuel oil system.

NOTE: In diesel mode operation the ignition fuel system is always active.

Fuel fine filter (duplex filter) DF1 (fitted)

Duplex change over type (mesh size of $25 \mu m$) is fitted on the engine.

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5.1.3 External fuel oil system

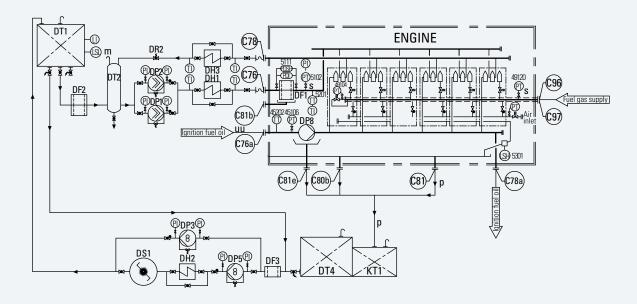


Fig. 5-1 External fuel oil system diagram with intermediate tank

DF1	Fuel fine filter (duplex filter)	C76	Duplex filter, inlet
DF2	Fuel primary filter (duplex filter)	C76a	Pilot fuel, inlet
DH3	Diesel oil cooler	C78	Fuel outlet
DP1	Diesel oil feed pump	C78a	Ignition fuel, outlet
DP2	Diesel oil stand-by feed pump	C80b	Drip fuel connection
DP8	Common rail high pressure pump		(sealing oil injection pump)
DR2	Fuel pressure regulating valve	C81	Drip fuel connection
DT1	Diesel oil day tank	C81b	Drip fuel connection
DT2	Diesel oil intermediate tank	C81e	Drip fuel connection, pilot fuel
KT1	Drip fuel tank	C96	Gas inlet
		C97	Flushing connection gas pipe (inert gas)
LI	Level indicator	m	Lead vent pipe beyond service tank level.
LSH	Level switch high	p	Free outlet required.
LSL	Level switch low	S	Please refer to the measuring point list
PDI	Diff. pressure indicator		regarding design of the monitoring devices.
PDSH	Diff. pressure switch high	uu	Only MDO fuel types DMA and DMZ acc. to
PI	Pressure indicator		ISO 8271 are to be used. For usage of DMB or
PT	Pressure transmitter		DMX please consult Caterpillar Motoren in
TI	Temperature indicator		advance.
TT	Temperature transmitter (PT100)		

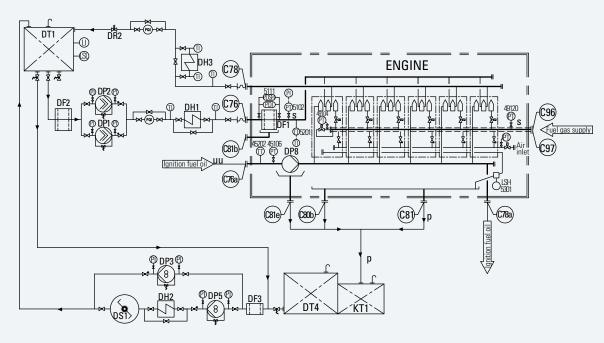


Fig. 5-2 External fuel oil system diagram without intermediate tank

Fuel fine filter (duplex filter)	C76	Duplex filter, inlet
Fuel primary filter (duplex filter)	C76a	Pilot fuel, inlet
Gas oil cooler	C78	Fuel outlet
Diesel oil feed pump	C78a	Ignition fuel, outlet
Diesel oil stand-by feed pump	C80b	Drip fuel connection
Common rail high pressure pump		(sealing oil injection pump)
Fuel pressure regulating valve	C81	Drip fuel connection
Diesel oil separator	C81b	Drip fuel connection
Diesel oil day tank	C81e	Drip fuel connection, pilot fuel
Diesel oil storage tank	C96	Gas inlet
Drip fuel tank	C97	Flushing connection gas pipe (inert gas)
Flow quantity indicator	p	Free outlet required.
Level indicator	S	Please refer to the measuring point list
Level switch high		regarding design of the monitoring devices.
Diff. pressure indicator	uu	Only MDO fuel types DMA and DMZ acc. to
Diff. pressure switch high		ISO 8271 are to be used. For usage of DMB or
Pressure indicator		DMX please consult Caterpillar Motoren in
Pressure transmitter		advance.
Temperature indicator		
	Fuel primary filter (duplex filter) Gas oil cooler Diesel oil feed pump Diesel oil stand-by feed pump Common rail high pressure pump Fuel pressure regulating valve Diesel oil separator Diesel oil day tank Diesel oil storage tank Drip fuel tank Flow quantity indicator Level indicator Level switch high Diff. pressure indicator Diff. pressure switch high Pressure indicator Pressure transmitter	Fuel primary filter (duplex filter) Gas oil cooler Diesel oil feed pump C78a Diesel oil stand-by feed pump C80b Common rail high pressure pump Fuel pressure regulating valve Diesel oil separator C81b Diesel oil day tank C81e Diesel oil storage tank C96 Drip fuel tank C97 Flow quantity indicator Level indicator Level switch high Diff. pressure indicator Pressure indicator Pressure transmitter

Temperature transmitter (PT100)

 TT

General

The design of the fuel oil system may vary from ship to ship, the system itself has to provide sufficient, permanent and clean fuel oil of the required viscosity and pressure to each engine. Fuel storage, treatment, temperature and pressure control as well as sufficient circulation must be ensured.

Diesel oil storage tank DT4

The tank design, sizing and location are according to classification society requirements and based on ship application. No heating is necessary because all marine distillate fuels are suitable for pumping.

Diesel oil separator DS1

Depending on the fuel oil quality a diesel oil separator DS1 is recommended for the use of MGO and required for MDO by Caterpillar Motoren. Any fuel oil must always be considered as contaminated upon delivery and should therefore be thoroughly cleaned to remove solid and liquid contaminants before use. Most of the solid contaminants in the fuel are rust, sand, dust.

Liquid contaminants are mainly water, i.e. fresh water or salt water.

Impurities in the fuel oil can result in

- · damage to fuel injection pumps and injectors,
- increased cylinder liner wear,
- deterioration of the exhaust valve seats
- increased fouling of turbocharger blades.

If a diesel oil separator is installed a total diesel oil separator capacity of 100 % of the full load fuel consumption is recommended.

HT-water or electrical heating is normally used as heating medium.

The nominal capacity should be based on a separation time of 22h/day:

$$V_{\text{eff.}}[\text{I/h}] = 0.28 \cdot P_{\text{eng.}}[\text{kW}]$$
 $V_{\text{eff.}} = \text{Volume effective [I/h]}$ $P_{\text{eng.}} = \text{Power engine [kW]}$

Diesel oil day tank DT1

The day tank collects clean / treated fuel oil, compensates irregularities in the treatment plant and its standstill periods. Two day tanks are to be provided, each with a capacity according to classification rules. The tank should be provided with a sludge space including a sludge drain valve and an overflow pipe from the MDO/MGO service tank to the settling/storage tank. The level of the tank must ensure a positive static pressure on the suction side of the fuel feed pumps. Usually tank heating is not required.

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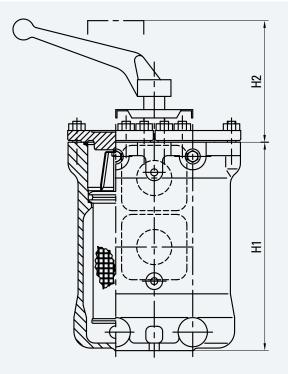
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Fuel primary filter (duplex filter) DF2

The fuel primary filter protects the fuel meter and feed pump from major solids. A duplex change over type with mesh size of 320 μ m is recommended.



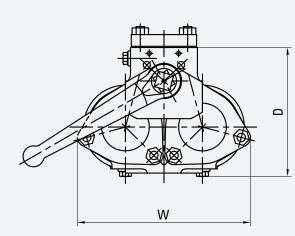


Fig. 5-3 Fuel primary filter DF2

Engine output	DN	Dimensions [mm]					
[kW]	DIN	H1	H2	W	D		
≤ 10,000	65	523	480	260	355		
≤ 20,000	80	690	700	370	430		

Flow quantity indicator FQI

One fuel meter is sufficient if the return fuel from the engine is connected to the diesel intermediate tank DT2.

If the fuel return from engine is connected to the day tank, an additional fuel meter in the return line to day tank has to be provided.

A minimum static fuel pressure head of at least 0.2 bar has to be considered. The fuel may be provided by gravity flow from the day tank. The static pressure must exceed the back pressure of the flow meter and prefilter.

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Diesel oil intermediate tank DT2

In the intermediate tank DT2 the warm return fuel from the engine mixes with the fuel from the day tank. The tank shall be vented as an open system, with the ventilation line guided to above the day tank level.

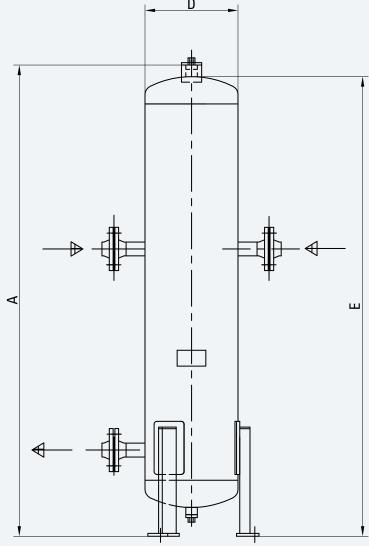
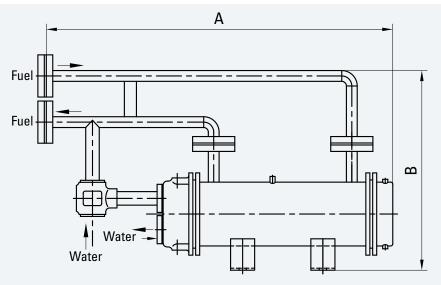


Fig. 5-4 Diesel oil intermediate tank DT2

Plant output	Volume	Ī	Weight		
[kW]	[1]	А	D	Е	[kg]
≤ 10,000	100	1,700	323	1,500	120
> 10,000	200	1,700	406	1,500	175

Diesel oil preheater DH1 (hot water)



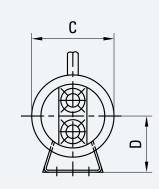


Fig. 5-5 Diesel oil preheater DH1

Engino		Dimensions [mm]							
Engine	А	В	С	D	[kg]				
6-9 M 46 DF	1,468	484	Ø 205	140	ca. 75				

The capacity of the MDO preheater is to determine on the required fuel temperature up to approx. 50 °C.

Heating capacity: $Q[kW] = \frac{P_{eng.}[kW]}{166}$

Q = Heating capacity [kW] $P_{eng} =$ Power engine [kW]

A diesel oil preheater is not required

- for gas oil operation.
- with preheated day tanks.

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Feed pump DP1/DP2 (separate)

The feed pump DP1/DP2 delivers fuel through the filter DF1 to each injection pump.

The feed pump maintains the pressure at the injection pumps and circulates the fuel in the system.

The capacity is slightly oversized to transfer the heat, which occurs during the injection process, away from the fuel injection system.

A positive static pressure is required at the suction side of the pump.

Capacity see technical data.

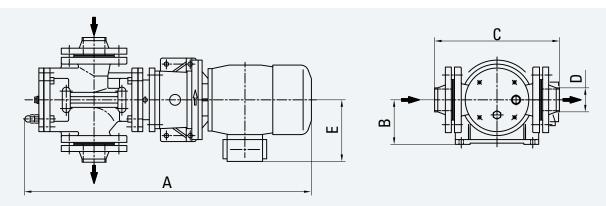


Fig. 5-6 Feed pump DP1/DP2

Engine		Dime	nsions	[mm]		Weight	Motorpower	Voltage / Frequency
	А	В	С	D	Е	[kg]	[kW]	[V/Hz]
6-9 M 46 DF	805	132	314	60.3	180	72	3.0	400/50
6 M 46 DF	775	132	314	60.3	180	70	2.6	440/60
7/8/9 M 46 DF	805	132	314	60.3	180	72	3.6	440/60

Fuel oil cooler DH3

To ensure a fuel oil temperature below 50 °C at any time a cooling of diesel oil may be required. The need for a fuel cooler is system specific and depends on fuel circuit design and type of fuel oil. In case of more than one engine connected to the same fuel supply system, the MDO-cooler capacity has to be increased accordingly.

The heat transfer load into the diesel oil system is approx. 3.1 kW/cyl.

LT-water is normally used as cooling medium.

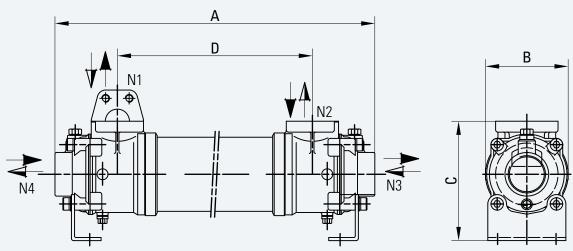


Fig. 5-7 Fuel oil cooler for MDO operation DH3

Engino		Weight					
Engine	А	В	С	D	N1 + N2	N3 + N4	[kg]
6-9 M 46 DF	940	148	225	702	DN50	1 ½" BSP	39

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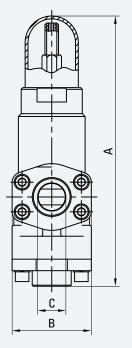
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Fuel pressure regulating valve DR2

To ensure a sufficient diesel oil pressure at engine inlet, a fuel pressure regulating valve DR2 has to be installed and adjusted during commissioning of the engine.



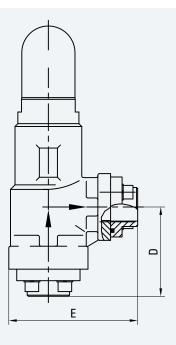


Fig. 5-8 Fuel pressure regulating valve

Plant output	Dimensions Imml								
[kW]	А	В	С	D	Е	[kg]			
≤ 6,000	248	70	Ø 25	88	122.5	3.6			
> 6,000	279	94	Ø 38	109	150.5	8.4			

5.2 HFO operation

The following section is based on the experiences gained in the operation of heavy fuel installations. Stable and correct viscosity of the fuel before injection pumps (see technical data) must be maintained at any time. Sufficient circulation through every engine connected to the same circuit must be ensured in all operating conditions.

The fuel treatment system should comprise at least one settling tank and two separators.

Correct dimensioning of HFO separators is of great importance, and therefore the recommendations of the separator manufacturer must be closely followed.

Poorly purified fuel is harmful to the engine. A high content of water may also damage the fuel feed system.

Injection pumps generate pressure pulses into the fuel feed and return piping. The fuel pipes between the feed unit and the engine must be clamped properly to rigid structures. The distance between the fixing points should be at close distance next to the engine. (See chapter piping design, treatment and installation.)

ATTENTION:

In multiple engine installations, where several engines are connected to the same fuel feed circuit, it must be possible to close the fuel supply and return lines connected to the engine individually. (This is a SOLAS requirement.)

NOTE:

It is further stipulated that the means of isolation shall not affect the operation of the other engines, and it shall be possible to close the fuel lines from a position that is not rendered inaccessible due to fire on any of the engines.

In HFO mode operation the ignition fuel system is always active.

Fuel oil system

A pressurized fuel oil system, as shown in Fig. 5-10, is necessary when operating on high viscosity fuels. When using high viscosity fuels requiring high preheating temperatures, the fuel oil from the engine fuel oil system to the return line will also have a relatively high temperature. The fuel oil pressure measured on the engine (at fuel pump level) should be about 5 bar. This maintains a pressure margin against gasification and cavitation in the fuel system, even at 150 °C preheating.

In order to ensure correct atomization, the fuel oil temperature must be adjusted according to the specific fuel oil viscosity used. An inadequate temperature can influence the combustion and could cause increased wear on cylinder liners and piston rings, as well as deterioration of the exhaust valve seats. A too low heating temperature, i.e. too high viscosity, could also result in excessive fuel consumption. Therefore, optimum injection viscosity of 10-12 cSt must be maintained at any rate and with all fuel grades.

Deviations from design recommendations are possible, however, they should be discussed with Caterpillar Motoren.

Trace heating for all heavy fuel pipes is recommended.

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Viscosity temperature sheet

Viscosity temperature sneet

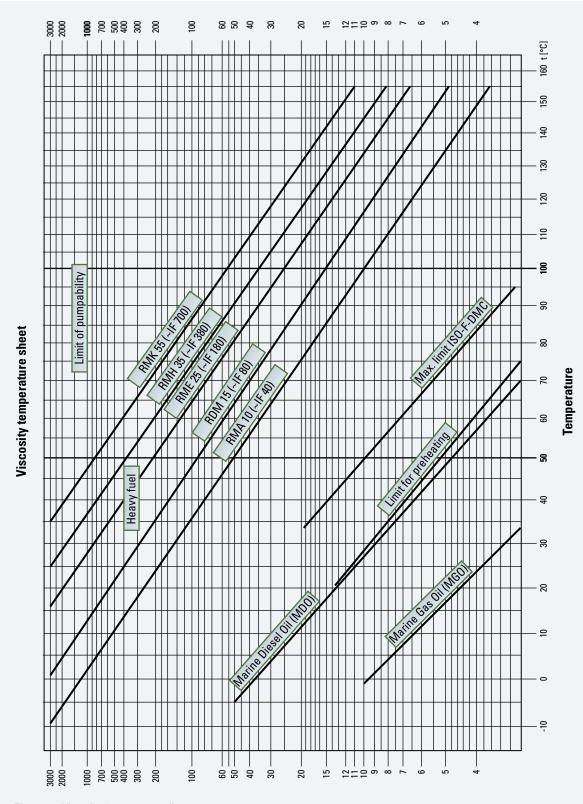


Fig. 5-9 Viscosity / temperature diagram

5.2.1 CIMAC – Requirements for residual fuels for diesel engines (as delivered)

Fuel shall be free of used lube oil.

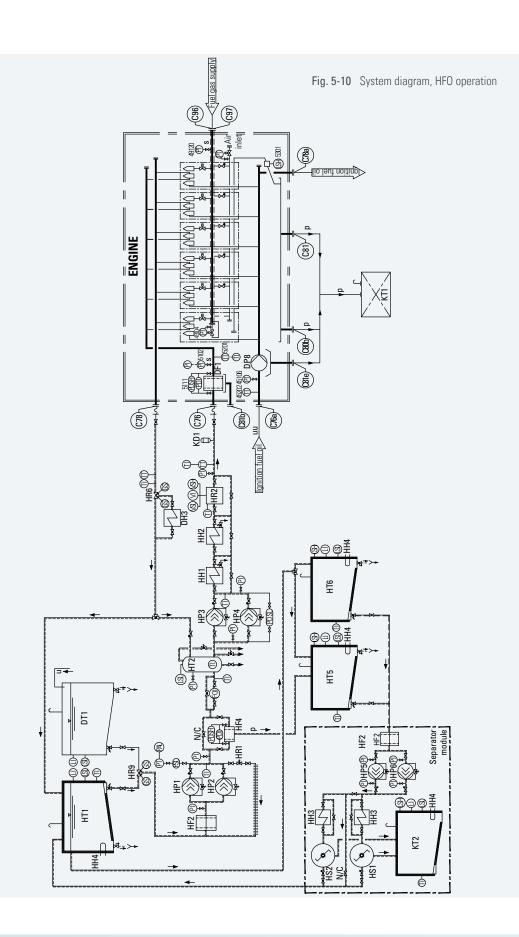
CIMAC CIMAC	RMH RMK 700 700	nent	991 1,010	r resid	ual fue	els fo	or diese	el engir	nes ZZ	0.15	0.10	e tab	3.5	ext 450	page.	15	15	30
CIMAC CIMAC H45 K45			991 1,010	45		09		30	22	0.15	0.10	0.5	3.5	450	09	15	15	30
CIMAC	K35 RMK 380 1,010							22	0.15				450					
C CIMAC H35	_		991	35		09		30			0.10	0.5	3.5	350	09	15	15	30
C CIMAC									18	0.15				350				
C CIMAC F25	<u> </u>	25		09		30	20	0.15	0.10	0.5	3.5	200	20	15	15	30		
C CIMAC F25			4)		15 5)		9		15	0.10				150				
C CIMAC			980 4)	15		09		30	14	0.10	0.10	0.5	3.5	150	40	15	15	30
C CIMAC			975 3)					24	14					300				
C CIMAC B10	+			10		09	0	9	12 6)	0.10	0.10	0.5	3.5	150	40	15	15	30
CIMAC			950 2)		9													
Designation	Related to ISO8217 (12) F-	Limit	max	max	mim	min	max	тах.	n) max	(n	(r) max	ı) max	max	max	max	max	max
_ Desig	Rela IS0821	Dim.	kg/m³	cSt. 1)	cSt. 1)	J _o	ွ	၁့	(m/m) %	(m/m) %	(m/m) %	(VV) %	(m/m) %	mg/kg	mg/kg	mg/kg	mg/kg	ma/ka
	Characteristic		Density at 15°C	Kin. viscosity at 100°C	Kin. viscosity at 100°C	Flash point	Pour point winter	Pour point summer	Carbon residue	Ash	Total sedim. after ageing	Water	Sulphur	Vanadium	Aluminum + Silicon	Zink	Phosphor	Calcium

2) ISO: 960 / 3) ISO: 960 / 4) ISO: 975 / 5) ISO: not limited / 6) ISO: carbon residue 10 Kinematic viscosity at 100°C [mm²/s] (cSt.) Kinematic viscosity at 50°C [mm²/s] (cSt.) Kinematic viscosity at 100°F Redw. [I sec.]

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General

For location, dimensions and design (e.g. flexible connection) of the disconnecting points see engine installation drawing.

No valve fittings with loose cone must be installed by the shipyard in admission and return lines.

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Storage tanks

The tank design, sizing and location must comply with classification society requirements and are based on ship application.

Heating coils are necessary and are to be designed so that the HFO temperature is at least 10K above the pour point to ensure a pumping viscosity below 1,000 cSt.

Heating is possible by steam, thermal oil, electrical current or hot water.

Settling tanks HT5, HT6

The tank design, sizing, location must comply with classification society requirements and are based on ship application. Two settling tanks are to be provided.

Its function is to remove water and solids by gravity due to higher fuel oil temperature and reduced turbulences. Provide constant oil temperature and avoid interruption of treatment system, due to overflow from HFO day tank. Thermal insulation of the settling tanks is recommended to avoid heat losses.

In order to ensure a sufficient settling effect, the following settling tank designs are permitted:

- 2 settling tanks, each with a capacity sufficient for 24 hours full load operation of all consumers or
- 1 settling tank with a capacity sufficient for 36 hours full load operation of all consumers and automatic filling

Settling tank temperature shall be 70 - 80 °C; the charging level shall be 70 - 90 %.

Heavy fuel preheater (separator) HH3

Heavy fuel oil needs to be heated up to a certain temperature before separating.

The most common heaters on board of ships are steam heaters. Other fluid heating sources are hot water, thermal oil or electrical heaters. Overheating of the fuel may cause fuel cracking. Thus the maximum electric load on the heater element should not exceed 1 Watt/cm².

In a cleaning system for HFO the usual processing temperature is 98 °C.

The separator manufacturer's guidelines have to be observed.

Heavy fuel transfer pumps (separator) HP5, HP6

The separator feed pumps shall be installed as close as possible to the settling tanks.

The separator manufacturer's guidelines have to be observed.

Heavy fuel separators HS1, HS2

Any fuel oils whether heavy fuel oil, diesel oil or crude oil must always be considered as contaminated upon delivery and should therefore be thoroughly cleaned before use.

Therefore self-cleaning types should be selected.

The purpose of any fuel treatment system is to clean the fuel oil by removal of water, solids, and suspended matter to protect the engine from excessive wear and corrosion.

Liquid contaminants are mainly water, i.e. either fresh water or salt water.

Impurities in the fuel can cause damage to fuel injection pumps and injectors, and can result in increased cylinder liner wear and deterioration of the exhaust valve seats as well as increased fouling of turbocharger blades.

Two separators with independent electrically driven pumps must be provided.

Separator sizing:

The correct sizing of the separators is based on the max. fuel oil consumption at maximum continuous rating (MCR) of the engines. The following formula can be used:

(The fuel consumption of auxiliary engines and boilers, if there are any, must be included)

$$V_{off} = 0.28 P (I/h)$$

 $V_{eff.} = Volume effective [I/h]$

 $P_{...} = Power engine [kW]$

The cleaning capacity of the separator must always be higher than the entire fuel consumption of the plant, incl. aux. equipment.

ATTENTION:

The separator outlet pressure is limited, so the pressure in the pipe line between separator outlet and day tank must be observed carefully. Follow the separator manufacturer's guidelines.

Heavy fuel day tank HT1

The tank design, sizing and location must comply with classification society requirements based on ship application. Two day tanks are to be provided. Each day tank capacity must be designed for full load operation of all consumers according to classification requirements. An overflow system into the settling tanks is required.HFO day tanks shall be provided with heating coils and sufficient insulation. Heating is possible by steam, thermal oil or hot water. The day tank temperature shall be above 90 °C.

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5.2.2 Fuel booster and supply system

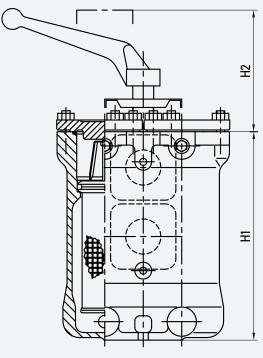
The booster system shall provide a pre-pressure to the mixing tank of approx. 4 - 5 bar. The circulating system provides sufficient flow of the required viscosity to the injection pumps. The circulation flow rate is typically 3.5 - 4 times the fuel consumption at MCR to prevent overheating of the fuel injection system and thus avoiding evaporation in the injection pumps.

Fuel change over main valve HR9

A manually operated three-way valve for changing over from MDO/MGO to HFO operation and back to MDO/MGO equipped with limit switches is necessary.

Primary filter (duplex filter) HF2

A protection strainer with a mesh size 320 μ m has to be installed before fuel pressure pumps to prevent any large particles entering the pump.



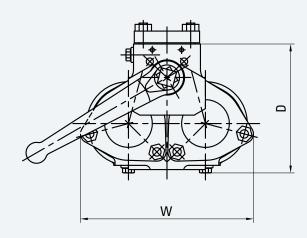


Fig. 5-11 Primary filter HF2

Engine output	DN	Dimensions [mm]						
[kW]	DIN	H1	H2	W	D			
≤ 10,000	40	330	300	250	210			
≤ 20,000	65	523	480	260	355			
> 20,000	80	690	700	370	430			

Fuel pressure pump HP1, fuel stand-by pressure pump HP2

Two supply pumps in parallel are recommended, one in operation and one on stand-by.

The capacity of the pump must be sufficient to prevent pressure drop during flushing of the automatic filter.

A suction strainer with a mesh size of 320 µm should be installed before each pump.

- Screw type pump with mechanical seal.
- Vertical or horizontal installation is possible.
- Delivery head 5 bar.

Capacity
$$V [m^3/h] = 0.4 \cdot \frac{P_{eng.} \cdot [kW]}{1,000}$$
 $V = Volume [m^3/h]$ $P_{eng.} = Power engine [kW]$

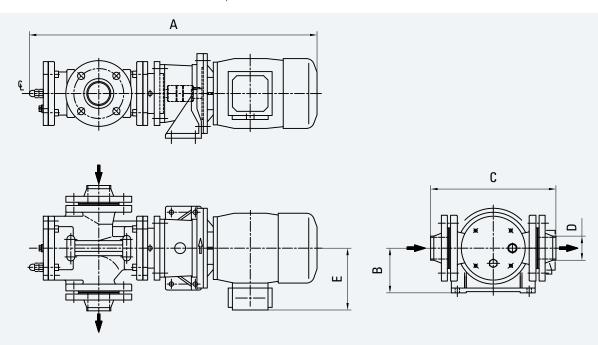


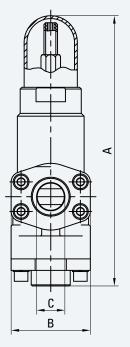
Fig. 5-12 Fuel pressure pump HP1; fuel stand-by pressure pump HP2

Plant output		Dir	ım]		Weight	Voltage / frequency	
[kW]	А	В	С	D	Е	[kg]	[V/Hz]
5,400 - 7,720	775	132	314	60.3	180	70	400/50
8,100 - 11,580	805	132	314	60.3	180	72	400/50
13,510	820	132	314	60.3	190	80	400/50
14,400 - 17,370	980	160	354	88.9	210	124	400/50

Plant output		Dir	Weight	Voltage / frequency			
[kW]	А	В	С	D	Е	[kg]	[V/Hz]
5,400 - 8,685	775	132	314	60.3	180	70	440/60
10,800 - 13,510	805	132	314	60.3	180	70	440/60
14,400 - 17,370	820	132	314	60.3	190	80	440/60

Fuel pressure regulating valve HR1

This valve is installed for adjusting a constant and sufficient pressure at engine fuel inlet. Due to the overcapacity of the pressure pumps HP1/HP2 the valve provides a nearly constant pressure under all operating conditions - from engine stop to maximum engine consumption. For MD0/MG0 operation the pipes of the fuel return line must be equipped with sufficient fincoolers to reduce the generated heat.



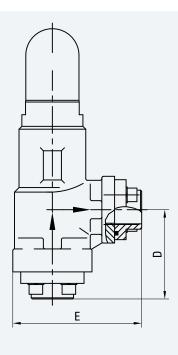


Fig 5-13 Fuel pressure regulating valve

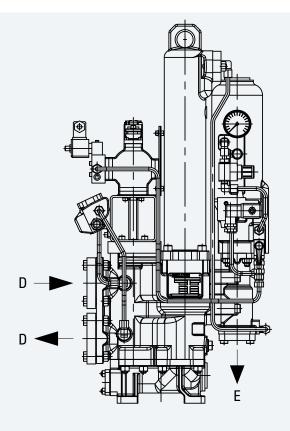
Plant output	Dimensions Imml								
[kW]	А	В	С	D	Е	[kg]			
≤ 8,400	248	70	Ø 25	88	122.5	3.6			
> 8,400	279	94	Ø 38	109	150.5	8.4			

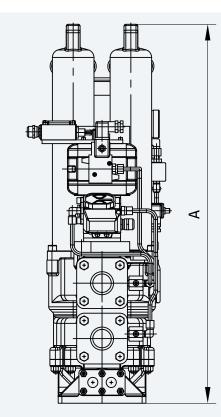
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HFO automatic filter **HF4**

An automatic filter with a mesh size 10 μ m (absolute) is required to remove cat fines from the fuel oil. The filter is installed between day tank and mixing tank.





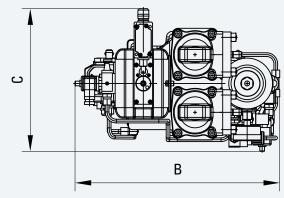


Fig. 5-14 HFO automatic filter HF4

Plant output	Dimensions [mm]								
[kW]	А	В	ВС		E				
≤ 12,000	890	520	335	DN 65	DN 50				
≤ 19,800	975	590	410	DN 80	DN 65				

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Flow quantity indicator FQ1

The fuel meter has to be installed between feed pumps and mixing tank HT2. Independent fuel consumption measurements for individual engines can be provided by installing two flow meters per engine, one at the feed line and one at the return line.

Mixing tank HT2

The mixing tank acts as a buffer for fuel viscosity and/or fuel temperature, when changing over from HFO to diesel oil and vice versa. In the mixing tank the warm return fuel from the engine is mixed with the fuel delivered from the day tank.

Venting to the day tank is required, if level switch is activated, due to accumulated air or gases in the mixing tank.

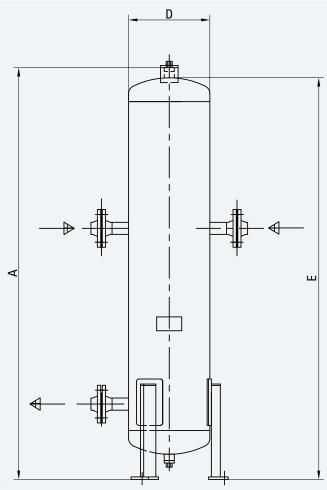


Fig. 5-15 Mixing tank HT2

Plant output	Volume	١	Weight		
[kW]	[1]	А	D	Е	[kg]
≤ 10,000	100	1,700	323	1,500	120
> 10,000	200	1,700	406	1,500	175

Fuel circulating pump HP3, stand-by circulating pump HP4

Two fuel circulating pumps in parallel are recommended, one in operation and one on stand-by. The circulating pumps maintain the required fuel circulation through the engine's fuel injection system.

- Screw type pump with mechanical seal
- Vertical or horizontal installation is possible
- Delivery head 5 bar

$$\begin{array}{lll} \text{Capacity} & \text{V [m³/h]} = 0.7 \cdot \frac{P_{\text{eng.}} \cdot [\text{kW}]}{1,000} & \text{V =} & \text{Volume [m³/h]} \\ & P_{\text{eng.}} = & \text{Power engine [kW]} \end{array}$$

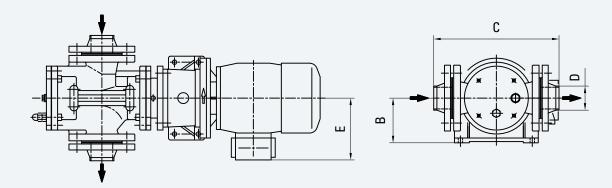


Fig. 5-16 Fuel circulating pump HP3, Stand-by circulating pump HP4

Plant output		Dir	Weight	Voltage / frequency			
[kW]	А	В	С	D	E	[kg]	[V/Hz]
≤ 6,300	805	132	314	60.3	180	72	400/50
≤ 8,100	820	132	314	60.3	190	80	400/50
≤ 12,600	980	160	354	88.9	210	124	400/50
≤ 17,370	1,020	160	354	88.9	210	139	400/50

Plant output	lant output Dimensions [mm]						
[kW]	А	В	С	D	Е	[kg]	[V/Hz]
≤ 5,400	775	132	314	60.3	180	70	440/60
≤ 8,100	805	132	314	60.3	180	72	440/60
≤ 12,600	820	132	314	60.3	190	80	440/60
≤ 17,370	980	160	354	8.9	210	124	440/60

Heavy fuel final preheater HH1, stand-by final preheater HH2

The capacity of the final preheater shall be determined based on the injection temperature at the nozzle, to which 4 K must be added to compensate for heat losses in the piping.

The piping for both heaters shall be arranged for separate and series operation.

Parallel operation with half the flow must be avoided due to the risk of sludge deposits.

The arrangement of only one preheater may be approved where it is ensured that the operation with fuel oil which does not need preheating can be temporarily maintained.

NOTE:

Safe return to port requirement, maneuverability must be ensured.

- Two mutually independent final preheaters have to be installed.
- The arrangement of only one preheater may be approved where it is ensured that the operation with fuel oil which does not need preheating can be temporarily maintained.

Heating media:

- Electric current (max. surface power density 1.1 W/cm²)
- Steam
- Thermal oil

Temperature at engine inlet max. 150 °C

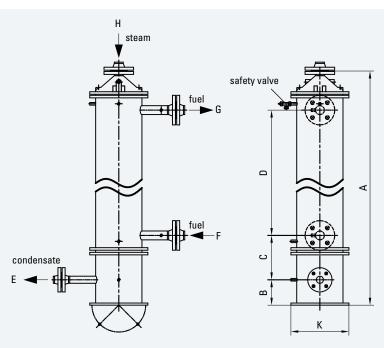


Fig. 5-17 Heavy fuel final preheater HH1, stand-by final preheater HH2 (steam heated)

Plant output	Dimensions [mm]							Weight		
[kW]	А	В	С	D	Е	F	G	Н	K	[kg]
up to 5,400	1,520	120	210	1,005	DN 25	DN 32	DN 32	DN 32	Ø 275	155
up to 8,800	2,065	120	215	1,540	DN 25	DN 40	DN 40	DN 32	Ø 275	272
up to 14,000	1,630	130	235	1,035	DN 40	DN 50	DN 50	DN 50	Ø 390	265
up to 21,000	2,170	130	235	1,555	DN 40	DN 65	DN 65	DN 50	Ø 390	339

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Viscosimeter HR2

The viscosimeter is regulating in conjunction with the final preheater the required fuel injection viscosity. This device automatically regulates the heating of the final preheater depending on the viscosity of the bunkered fuel oil, so that the fuel will reach the nozzles with the viscosity required for injection.

Pressure absorber KD1 (optional)

During the injection phases of fuel from the supply line, compression and injection as well as the release of unused fuel into the return line, cyclic pressure pulsations may result. The requirement of installing fuel dampers in the external pipe system depends on the design of the external fuel pipe work and its ability to absorb such pulsations sufficiently. Just in case of enhanced damping requirements additional dampers have to be installed.

Bypass overflow valve HV (optional)

If more than one engine is connected to the fuel booster and supply system a bypass overflow valve between the feed line and the return line can be required.

It serves to secure and stabilize the pressure in the fuel feed line under all circumstances and operation conditions. The overflow valve must be differential pressure operated.

The opening differential pressure should be 2 bar.

Duplex filter HF1 (fitted)

The fuel duplex filter is installed at the engine.

The two filter chamber construction allows continuous operation without any shut downs for cleaning the filter elements.

The drain connection of the filter is provided with a valve and must be routed to the leak oil tank. If the filter elements are removed for cleaning, the filter chamber must be emptied. This prevents the dirt particles remaining in the filter casing from migrating to the clean oil side of the filter.

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Fuel oil cooler DH3

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To ensure a fuel oil temp. below 50 °C a cooling of diesel oil may be required.

The need for fuel cooler is system specific and depends on fuel circuit design and type of fuel oil.

In case of more than one engine are connected to the same fuel supply system, the MDO-cooler capacity has to be increased accordingly.

The diesel oil coolers are always installed in the fuel return line (engine connection C78). The heat transfer load into the diesel oil system is approx. 3.1 kW/cyl. LT-water is normally used as cooling medium.

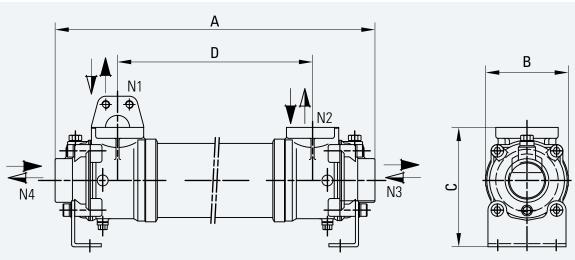


Fig. 5-18 Fuel oil cooler for MDO operation DH3

Fraire			Dimensio	ensions [mm]				
Engine	А	В	С	D	N1 + N2	N3 + N4	[kg]	
6-9 M 46 DF	940	148	225	705	DN50	1 ½" BSP	39	

5.2.3 Fuel booster and supply module

A complete fuel conditioning module, designed for HFO up to 700 cSt / 50 °C, can be supplied.

Caterpillar Motoren standard modules consist of the following components:

- Three-way change over valve
- Booster pumps
- Automatic filter
- Pressure regulating valve
- Fuel flow meter
- Mixing tank

- Circulating pumps
- Fuel preheater (steam, thermal oil or electric)
- Viscosity control
- Diesel oil cooler
- Control cabinet
- Alarm panel

Built on one frame, they include all piping, wiring and trace heating.

Module controlled automatically with alarms and starters

- Pressure pump starters with stand-by automatic
- Circulating pump starters with stand-by automatic
- Pl-controller for viscosity controlling
- Starter for the viscosimeter
- Analog output signal 4 20 mA for viscosity

Alarms

- Pressure pump stand-by start
- Low level in the mixing tank
- Circulating pump stand-by start
- Self-cleaning fine filter clogged
- Viscosity alarm high/low
- The alarms with potential free contacts
- Alarm cabinet with alarms to engine control room and connection interface for remote start/stop and
- indicating lamp of fuel pressure and circulating pumps

Size, weight and dimensions

The whole module is tubed and cabled up to the terminal strips in the electric switch boxes which are installed on the module. All necessary components like valves, pressure switches, thermometers, gauges etc. are included. The fuel oil pipes are equipped with trace heating (steam, thermal oil or electrical) where necessary.

NOTE:

The module will be tested hydrostatical and functional in the workshop without heating and not connected to the engine.

Fuel oil standard module

Madula siza	Capacity	Module size (LxWxH)	Module weight
Module size	up to [kW]	[mm]	[kg]
Size 1	1,900	2,800 x 1,200 x 2,100	1,700
Size 2	2,800	2,800 x 1,200 x 2,100	1,800
Size 3	4,200	3,000 x 1,200 x 2,100	2,200
Size 4	6,000	3,200 x 1,300 x 2,100	2,700
Size 5	8,200	3,200 x 1,300 x 2,100	2,700
Size 6	9,300	3,400 x 1,400 x 2,100	3,000
Size 7	11,400	3,600 x 1,400 x 2,100	3,400
Size 8	13,100	3,600 x 1,400 x 2,100	3,400
Size 9	15,900	4,200 x 1,600 x 2,100	3,800
Size 10	19,800	5,000 x 1,700 x 2,100	4,600
Size 11	26,000	6,000 x 2,000 x 2,100	5,600

NOTE:

Customized modules are possible on request.

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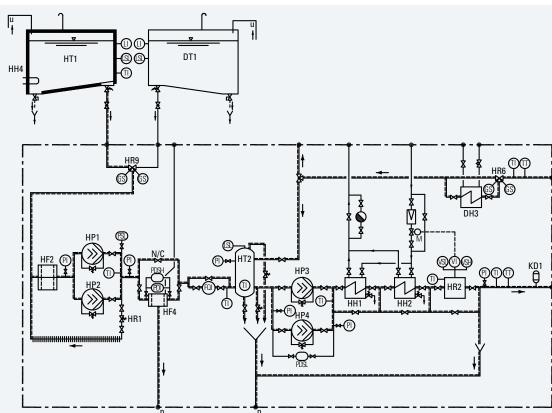
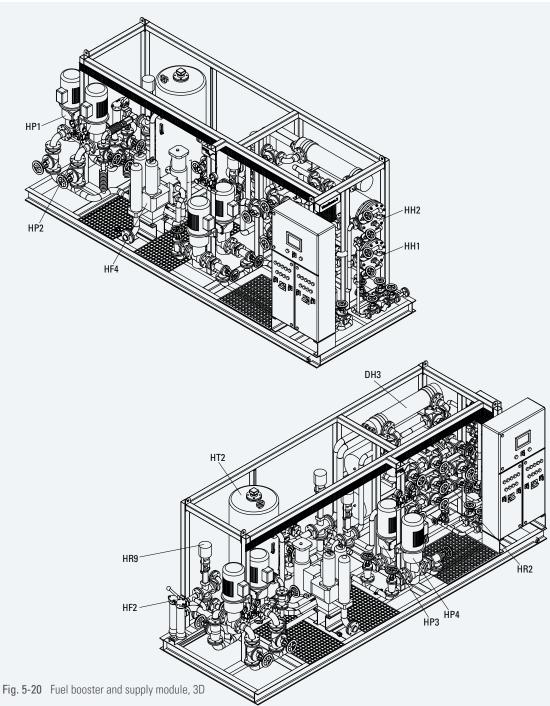


Fig. 5-19 Fuel booster and supply module, system diagram

DH3	Fuel oil cooler for MDO operation	KD1
DT1	Diesel oil day tank	FQI
HF2	Primary filter (duplex filter)	GS
HF4	HFO automatic filter	LI
HH1	Heavy fuel final preheater	LSL
HH2	Stand-by final preheater	PDI
HH4	Heating coil	PDS
HP1	Fuel pressure pump	PDS
HP2	Fuel stand-by pressure pump	PI
HP3	Fuel circulating pump	PSL
HP4	Stand-by circulating pump	TI
HR1	Fuel pressure regulating valve	TT
HR2	Viscosimeter	VI
HR6	Change over valve (HFO/diesel oil)	VSH
	3-way-valve	VSL
HR9	Fuel change over main valve	
HT1	Heavy fuel day tank	р
HT2	Mixing tank	u
All heav	yy fuel pipes have to be insulated.	

KD1	Pressure absorber
FQI	Flow quantity indicator
GS	Limit switch
LI	Level indicator
LSL	Level switch low
PDI	Diff. pressure indicator
PDSH	Diff. pressure switch high
PDSL	Diff. pressure switch low
PI	Pressure indicator
PSL	Pressure switch low
TI	Temperature indicator
TT	Temperature transmitter (PT100)
VI	Viscosity indicator
VSH	Viscosity control switch high
VSL	Viscosity control switch low
р	Free outlet required
u	Fuel separator or from transfer pump
	Heated pipe

FUEL OIL SYSTEM



HP1	Fuel pressure pump
HP2	Fuel stand-by pressure pump
HP3	Fuel circulation pump
HP4	Stand-by circulation pump
HR9	Fuel change over main valve
HT2	Mixing tank

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Coarse filter

Fuel oil cooler for MDO operation

Primary filter (duplex filter)

Heavy fuel final preheater Stand-by final preheater

HFO automatic filter

DH3

HF2 HF3

HF4

HH1

HH2

FUEL OIL SYSTEM

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5.3 Switching over from HFO to diesel oil

Continuous operation with HFO is recommended for engines designed for running mainly on HFO. Starting and stopping the engine on HFO (Pier to Pier) can be provided if a sufficient preheating of the fuel oil system is ensured.

The circulating pumps have to be permanently in service, so that a continuous circulation of warm/hot fuel oil through the engine is ensured.

A frequent change over from HFO to diesel oil is only recommended when necessary for flushing purposes, emergencies, special sea area emission requirements, etc.

Changing the fuel oil too quickly and too often may cause high risk of plunger seizure (thermal shock), fuel injection pump leakages, etc. in the fuel injection pump.

Only a slow switch over will attenuate that effect.

Typical switch over characteristics (HFO to diesel)

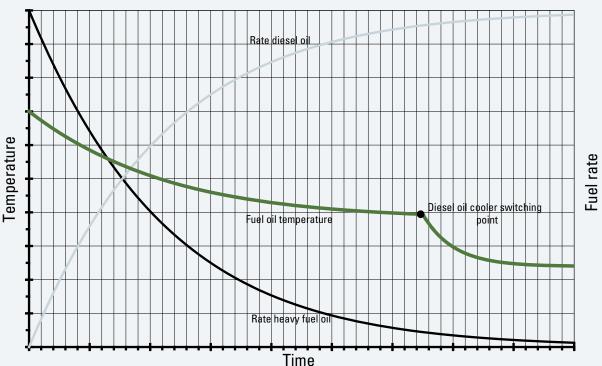


Fig 5-21 Switch over characteristics

6.1 General

The gas system provides the fuel gas from the Gas Valve Unit (GVU) to the gas admission valves on the engine.

The complete gas manifold on the engine is double walled and leak detected to comply with the gas safe machinery space requirements. A leakage location system to decrease the maintenance effort is available as an option.

The fuel gas will be port injected by solenoid gas valves, these gas valves are integrated in the cylinder head design.

The GVU is part of the Caterpillar Motoren standard scope of supply. One individual GVU per engine has to be provided. A maximum pipe length of 10 m between the GVU and the engine must not be exceeded. For applications, where the GVU is located directly in the machinery space, a gas-proof cover is available as an option to comply with the gas safe machinery space requirements.

6.1.1 Gas fuel quality requirements

Gas fuel to be complied with the Caterpillar gas fuel specification VD8768 for dual fuel engines.

Gas specification M 46 DF						
Gas temperature before engine inlet	[°C]	0 - 60				
Gas pressure before fuel regulating skid	[bar (g)]	6.5 - 9				
Maximum gas pressure fluctuation	[mbar/s]	+/- 80				
Minimum lower heat value	[MJ/m³]	28				
Minimum Cat - Methane number (without power derate)	[MN]	80				
Maximum Sulphur as H ₂ S	[mg/m³]	20				
Maximum Ammonia (NH ₄)	[mg/m³]	25				
Maximum Fluorines	[mg/m³]	Σ = 50				
Maximum Chlorine	[mg/m³]	Σ = 50				
Maximum oil content	[mg/m³]	50				
Maximum particles content	[mg/m³]	50				
Maximum particles size	[µm]	5				
Maximum tar content	[mg/m³]	10				
Maximum Silicium	[mg/m³]	10				
Maximum water		Saturated fuel or water and condensates at gas control unit are not allowed				

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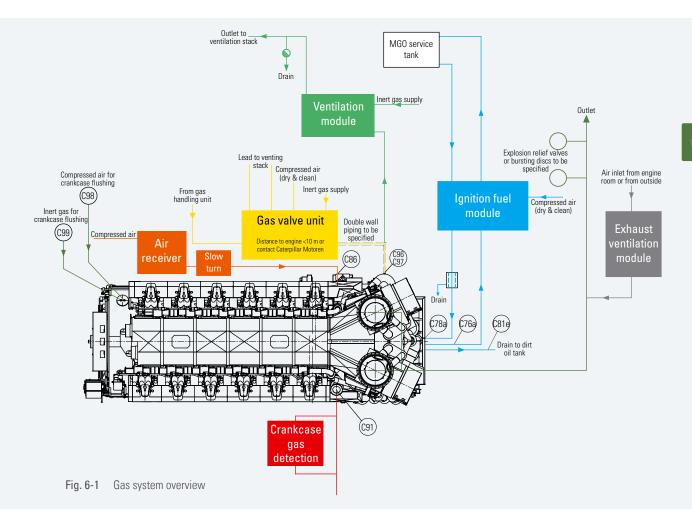
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6.1.2 Inert gas quality requirements

Inert gas to be complied with the Caterpillar inert gas specification VD8836 for dual fuel engines.

Inert gas specification M 46 DF						
Gas temperature range at interfaces to engine	[°C]	0 - 60				
Minimum pressure difference (min. inert gas - max. fuel gas)	[bar(g)]	1				
Maximum inert gas pressure	[bar(g)]	10				
Allowed gases		Nitrogen ≥ 95 % Carbon Dioxid 2.5				
Maximum Sulphur as H ₂ S	[%]	0,05 (= 770 mg/mn ³)				
Maximum Ammonia (NH ₃)	[mg/m³]	25				
Maximum Fluorines	[mg/m³]	Σ = 50				
Maximum Chlorine	[mg/m³]	$\Sigma = 50$				
Maximum oil content	[mg/m³]	50				
Maximum particles content	[mg/m³]	50				
Maximum particle size	[µm]	5				
Maximum dew point	[°C]	-20				

6.2 Gas system overview



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6.2.1 Gas valve unit (GVU)

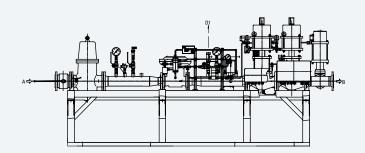
The gas valve unit provides the engine with the desired fuel gas pressure and fuel gas quantity. It is controlled by the engine's control and monitoring system and the engine's speed governor. The maximum distance between the GVU and the engine is 10 m. If more distance is requested please contact Caterpillar Motoren.

It has several features to safely cut the engine from the gas train and to remove the gas fuel from the piping system (flushing). In case of flushing the gas fuel is pushed by inert gas over the engine via the GVU towards the ship's vent system.

The shown GVU's are an example. GVU's can be supplied in horizontal and vertical design, as U-type and also mounted within an enclosure.

The gas valve unit is an off-engine component. GVU is single walled designed and needs to be installed in an ESD compliant machinery space or within an enclosure.

The GVU is optionally available with a gas fuel flow meter.





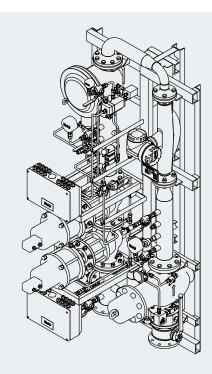


Fig. 6-3 Gas valve unit, U-form vertical

6.2.2 Ignition fuel system

The MaK dual fuel engine is equipped with an ignition fuel system to ignite the gas fuel / air mixture in the combustion chamber. This ignition system is a common rail system which injects only a small amount of MDO fuel.

Ignition fuel is to be used also during operation with liquid fuel, for cooling of injector needles. To achieve the cleanliness of the ignition fuel a filtering system is required.

6.2.2.1 Ignition fuel quality requirements

Only MDO fuel types DMA and DMZ acc. to ISO 8271 are to be used. For usage of DMB or DMX please consult Caterpillar Motoren in advance.

A filter module to provide the required ignition fuel cleanliness is part of MaK standard scope of supply.

6.2.2.2 Ignition fuel components

Ignition fuel module

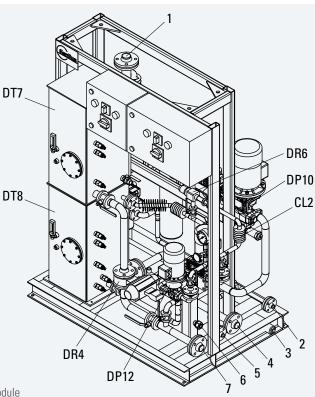


Fig. 6-4 Ignition fuel module

1	Vent to the top of day tank	CL2	Fin cooler
2	Return fuel from engine	DP10	Gear pump
3	Drain module	DP12	Gear pump
4	Drain filter and tank	DR4	Change over valve
5	DF to pilot injection system engine	DR6	Pressure regulating valve
6	Supply compressed air (dry & clean)	DT7	Mixing tank
7	DF from diesel oil day tank	DT8	Mixing tank

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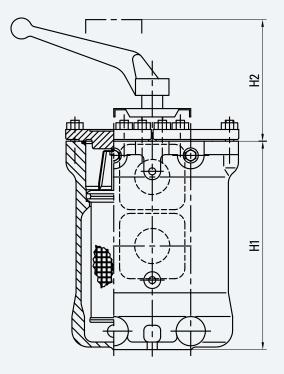
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Ignition fuel fine filter



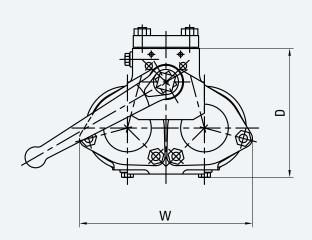


Fig. 6-5 Ignition fuel fine filter

Engine output	DN		Dimensio	ons [mm]	
[kW]	DIN	H1	H2	W	D
6-9 M 46 DF	25	200	170	206	ca. 150

Ignition fuel injector

Weight: 5.9 kg

The ignition fuel injector enables the injection of pressurized fuel directly into the cylinder.

The injector design is simple and compact, the key features are:

- Electronically controlled
- Flexible injection timing and duration
- Flow limiter



Fig. 6-6 Ignition fuel injector

High pressure pump

Weight: 36 kg

One high pressure pump delivers the required amount of ignition fuel to the injectors and provides the desired pressure in closed loop control. The pump itself is based on a proved design.



Fig. 6-7 High pressure pump

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6.2.3 Engine ventilation system

The ventilation module supplies permanent ventilation for continuous monitoring / leakage detection by vacuum pump and gas sensor. This pump is able to handle any kind of ignitable gases.

Nitrogen connection on the module, for flushing of the annular space of the double walled piping system and fuel gas supply line of the engine.

Depending on class requirements redundant equipment might be requested.

The standard design is for the use in an inherent safe engine room and is therefore of non-hazardous type.

The ventiltaion module shall be installed in the engine room as close as possible to the gas valve unit.

6.2.4 Engine ventilation module

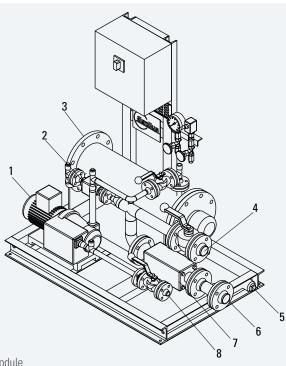


Fig. 6-8 Engine ventilation module

- 1 Vacuum pump
- 2 Electro-magnetic valve
- 3 Gas sensor
- 4 Jacketed pipe system, inlet Nitrogen, outlet
- 5 Drain module
- 6 Nitrogen, inlet
- 7 Electro-magnetic valve
- 8 Outlet to drain

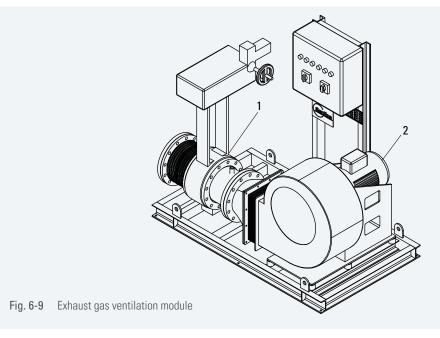
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6.2.5 Exhaust gas ventilation system

The exhaust gas ventilation module is installed to ventilate the ship side exhaust gas system after an emergency stop of the engine in gas mode. The module consists of a ventilation fan, a separated butterfly valve and exhaust gas compensator for the connection to the exhaust gas system. The butterfly valve separates the exhaust gas system under all conditions to protect the engine room against exhaust gas inrush except the case of a stop of the engine in gas mode. The ventilator is sized to remove the total volume of the exhaust gas system, incl. silencer, stack, boiler and duct three times. The engine start is blocked, if the valve is not completely closed, monitored by a position switch.

6.2.6 Exhaust gas ventilation module



- 1 Isolation valve
- Exhaust fan

6.2.7 Crankcase gas detection

The crankcase needs several protection devices to provide a reliable and safe operation of the dual fuel engine. Due to the normal blow-by special care needs to be taken to detect fuel gas before it reaches an explosive concentration.

This system detects an abnormal amount of fuel gas in the crankcase. The gas sensor will sense for fuel gas and will monitor the actual fuel gas concentration in percent of the lower explosion limit (% LEL). Before the LEL is reached an alarm will be triggered and without recovery of the LEL within a certain time, latest before the concentration of fuel gas will reach 100 % LEL, the engine will switch back to fuel oil to ensure that an explosive atmosphere will not occur due to fuel gas blow-by.

If abnormal blow-by occurs the pressure sensor will trigger an alarm, showing that at least one of the piston rings has worn and the switch over to fuel oil might occur soon.

A gas detection system might also be required to detect fuel gas in HT expansion tank and lube oil circulating tank, depending on authority.

6.2.8 Explosion relief valves for exhaust gas system

Exhaust gas piping in which explosive atmosphere can accumulate is routed steadily ascending to avoid gas accumulations. Additionally it is protected against overpressure by explosion pressure relief valves. These relief valves discharge the overpressure in case of any explosion within the exhaust gas system. The positioning and amount of explosion relief vavles must be adjusted according to the design and layout of the existing exhaust gas system.

In case of an explosion in the exhaust gas system the explosion relief valves open quickly. This reduces explosion overpressure inside the exhaust gas system to a safe level without any flame transmission to the surrounding area. After the explosion pressures subsides, the valves reseal, so that the engine could be restarted or further operated.

6.2.9 Slow turn

The slow turn module can turn the engine automatically in predefined intervals with pressure reduced starting air. This air supply is limited in such a way that the ignition engine speed will not be reached. A fuel injection will be disabled during this process. If the crankshaft will only start to oscillate during slow turning and will not come to a continuous rotation it must be assumed that water has accumulated in one of cylinders. In that case a starting interlock will be set For more information, please see also chapter 9.5

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6.3 Gas system – GVU inside gas safe machinery room

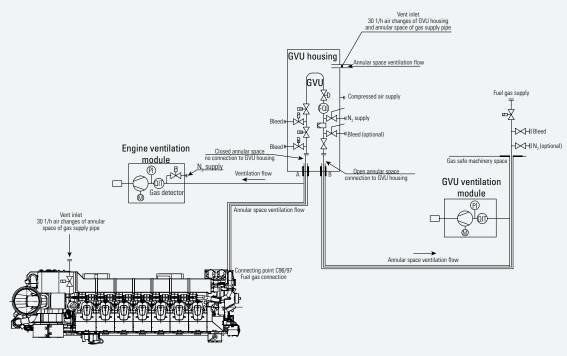


Fig. 6-10 Gas valve unit inside machinery room

6.3.1 GVU housing

In case of installing the GVU inside the machinery room and to ensure its definition as a safe machinery room the GVU needs to be encased and the gas pipe needs to be of double wall pipe.

The GVU housing is seen as an extension of the annular space of double wall fuel gas pipe in front of the GVU.

6.3.2 GVU ventilation module

Similar to the engine ventilation module the GVU ventilation module is used for permanent ventilation of the GVU housing and its double walled pipe inside machinery space.

The vent flow will be through the GVU housing and the annular space of the double wall fuel gas line by an explosion proofed fan. A gas detector will be installed close to the exhaust fans inside the extraction flow. The GVU housing is always connected to open atmosphere by the annular space and hereby not considered as a pressure vessel.

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General

The lube oil performs several basic functions:

- It cleans the engine by carrying dirt and wear particles until the filters can extract and store them.
- It cools the engine by carrying heat away from the piston, cylinder walls, valves and cylinder heads to be dissipated in the engine oil cooler.
- It cushions the engines bearings from the shocks of cylinder firing.
- It lubricates the wear surfaces, reducing friction.
- It neutralizes the corrosive combustion products.
- It seals the engines metal surfaces from rust.
- It lubricates the turbocharger bearings.
- It cools the injection nozzles.

7.1 Lube oil requirements

NOTE:

The viscosity class SAE 40 is required.

Wear and tear and thus the service life of the engine depend on the lube oil quality.

Therefore high requirements are made for lubricants:

- Constant uniform distribution of the additives at all operating conditions
- Perfect cleaning (detergent effect) and dispersing power, prevention of deposits from the combustion process in the engine
- Sufficient alkalinity in order to neutralize acid combustion residues
- The TBN (total base number) must be 30 KOH/g at HFO operation
 The TBN is 12 20 KOH/g for MDO operation depending on Sulfur content

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Manufacturer	Diesel oil / MDO operation	ı	II	HFO operation	ı	II
AGIP	DIESEL SIGMA S CLADIUM 120		X	CLADIUM 300 S CLADIUM 400 S	X	
ВР	ENERGOL HPDX 40 ENERGOL DS 3-154 ENERGOL IC-HFX 204 VANELLUS C3	X X X	X	ENERGOL IC-HFX 304 ENERGOL IC-HFX 404	X	
CAT	DEO	Х				
CHEVRON, CALTEX, TEXACO	DELO 1000 MARINE DELO SHP TARO 12 XD TARGO 16 XD TARGO 20 DP TARGO 20 DPX	X X X X		TARO 30 DP TARO 40 XL TARO 40 XLX	X X X	
CASTROL	MARINE MLC MHP 154 TLX PLUS 204	X X X		TLX PLUS 304 TLX PLUS 404	X	
CEPSA	KORAL 1540		Χ			
ESS0	EXXMAR 12 TP EXXMAR CM+ ESSOLUBE X 301	X	X	EXXMAR 30 TP EXXMAR 30 TP PLUS EXXMAR 40 TP EXXMAR 40 TP PLUS	X X	X
MOBIL	MOBILGARD 412 MOBILGARD ADL MOBILGARD M430 MOBILGARD 1-SHC ¹⁾ DELVAC 1640	X X X	X	MOBILGARD M430 MOBILGARD M440 MOBILGARD M 50	X X X	
SHELL	GADINIA GADINIA AL ARGINA S ARGINA T	X X X		ARGINA T ARGINA X	X	
TOTAL LUBMARINE	RUBIA FP DISOLA M 4015 AURELIA TI 4030 CAPRANO M40	X X X	Х	AURELIA TI 4030 AURELIA TI 4040	X	
LUKOIL	NAVIGO 12/40 NAVIGO 15/40	X		NAVIGO TPEO 30/40 NAVIGO TPEO 40/40	X	
GULF				SEA POWER 4030 SEA POWER 4040	X	

I Approved in operation / II Permitted for controlled use. When these lube oils are used, Caterpillar Motoren GmbH & Co. KG must be informed because at the moment there is insufficient experience available for engines. Otherwise the warranty is invalid. / 1) Synthetic oil with a high viscosity index (SAE 15 W/40). Only permitted if the oil inlet temperatures can be decreased by $5 - 10 \, ^{\circ}$ C.

7.2 Internal lube oil system

Lube oil force pump LP1 (fitted)

The lube oil force pump is a gear pump, fitted on the engine and mechanically driven by the crankshaft. The lube oil force pump provides the lube oil from the circulating tank LT1 to the engine.

It is designed to provide a sufficient amount of lube oil at the required pressure to the engine even when running at the designed minimum engine speed. Capacity, see technical data.

Duplex filter LF1 (fitted)

The duplex filter shall indicate a failure of the self-cleaning filter LF2.

Mesh size: 80 µm (absolute)

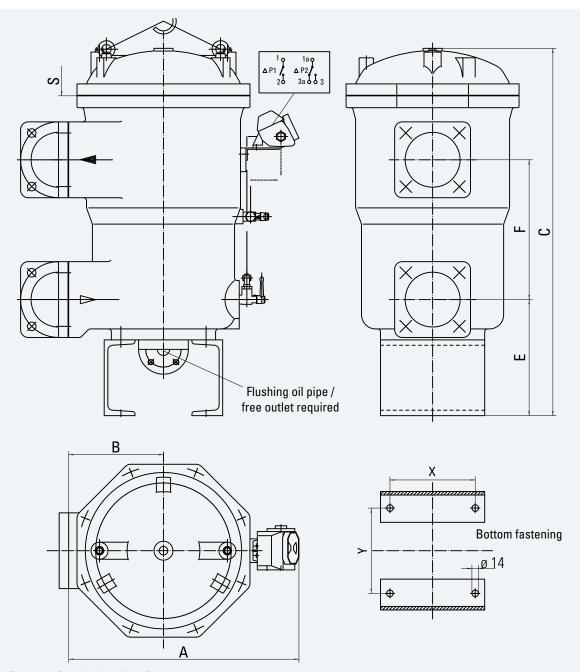
One chamber of the duplex filter is in operation, while the second chamber is in stand-by.

Change over can be done during engine operation.



Fig. 7-1 Self-cleaning lube oil filter LF2

Back flushing filter LF2 (separate), option



Back flushing filter LF2

	Dimensions [mm]							Weight	
	A B C E F S X Y							[kg]	
6/7 M 46 DF	580	260	950	245	350	600	220	220	195
8/9 M 46 DF	655	300	950	245	375	600	290	260	250

The back flushing filter protects the engine from dirt particles which may accumulate in the circulating tank LT1. Mesh size: 30 µm (absolute)

The filter is continuously flushing into the circulating tank without flushing oil treatment, without bypass filter.

7.3 External lube oil system

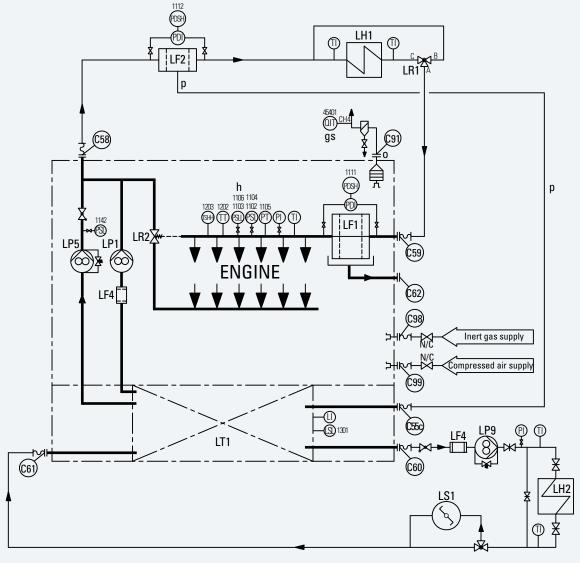


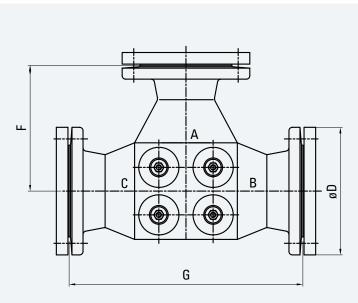
Fig. 7-3 External lube oil system diagram

LF1	Duplex lube oil filter	LP5	Prelubrication pump
LF2	Self-cleaning lube oil filter	LP9	Transfer pump (separator)
LF4	Suction strainer	LR1	Lube oil temperature control valve
LH1	Lube oil cooler	LR2	Oil pressure regulating valve
LH2	Lube oil preheater	LS1	Lube oil separator
LP1	Lube oil force pump	LT1	Sump tank

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Lube oil temperature control valve LR1

A wax operated control valve will be used to control the oil inlet temperature into the engine. It has an emergency manual adjustment. Option: Electric driven valve with electronical controller.



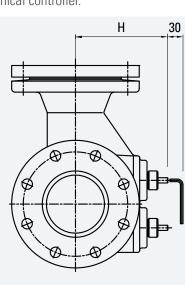


Fig. 7-4 Lube oil temperature control valve LR1

	Dimensions [mm]							
	DN	[kg]						
6/7 M 46 DF	125	250	241	489	200	67		
8/9 M 46 DF	150	150 285 254 489 200						

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Prelubricating pump LP5

This pump is mounted at the baseframe. This pump can only be used for prelubricating, not as stand-by for the force pump. Capacity see technical data.

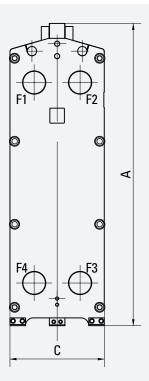
Oil pressure regulating valve LR2 (fitted)

The pressure control valve controls the lube oil pressure at engine inlet by giving only the adequate oil flow to the engine. Excessive oil flow will be led back into the engine oil pan.

Lube oil cooler LH1 (separate)

A plate cooler with plates of stainless steel will be used to dissipate the heat to the LT fresh water system. It is mounted at the baseframe

Option: separate



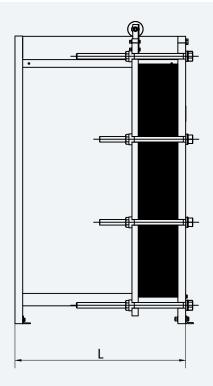




Fig. 7-5 Lube oil cooler LH1

	Dimensions						
	A B C D L					Weight	
	[mm]	[mm]	[mm]	[mm]	[mm]	[kg]	
6 M 46 DF	1,715	1,365	480	225	1,034	662	
7 M 46 DF	1,948	1,292	608	296	1,100	1,151	
8 M 46 DF	1,948	1,292	608	296	1,100	1,182	
9 M 46 DF	1,948	1,292	608	296	1,100	1,224	

Lube oil temperature control valve LR1 (electric driven valve), option

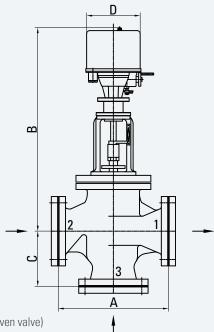


Fig. 7-6 Lube oil temperature

control valve LR1 (electric driven valve)

		Weight				
	DN A B C D					
6/7 M 46 DF	125	400	717	200	170	110
8/9 M 46 DF	150	480	742	240	170	149

Lube oil separator LS1 (separate)

The most effective cleaning of lube oil is carried out by means of separation.

Separation is mandatory for HFO driven plants and highly recommended for MGO/MDO operation.

Layout for MGO/MDO and gas operation

Automatic self-cleaning separator; Operating temperature 85 - 95 °C

$$V[I/h] = 0.18 \cdot P_{eng}[kW]$$

Layout for HFO and gas operation

Automatic self-cleaning separator; Operating temperature 95 °C

$$V[I/h] = 0.29 \cdot P_{eng}[kW]$$

For the layout of separators, please follow the separator manufacturer's guidelines.

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7.4 Circulating tanks

The circulating tank LT1 is mounted at the baseframe.

7.5 Crankcase ventilation system

7.5.1 Crankcase ventilation pipe dimensions

- The crankcase ventilation connecting point is DN 150.
- The engine main ventilation line must be at least DN 150.

7.5.2 Crankcase ventilation pipe layout

- The pipes should run upwards.
- Free ventilation under all trim conditions is required.
- To avoid backflow of condensate, a permanent drain of the ventilation pipe is required.

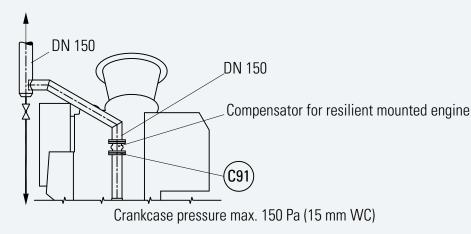


Fig. 7-7 Crankcase ventilation

C91 Crankcase ventilation to stack

7.5.3 Gas detection sensor

A gas detection sensor has to be installed in the crankcase vent pipe.

8.1 General

MaK engines are cooled by two cooling circuits:

- A high temperature (HT) and
- A low temperature (LT) cooling circuit

The cooling water needs to be treated according to Caterpillar Motoren requirements for MaK engines.

8.1.1 Two circuit cooling system

In this system arrangement, the two cooling systems are designed as two separate water circuits. Each circuit needs to be fitted with a header tank and a fresh water cooler.

8.1.2 Secondary circuit cooling system

In the "secondary circuit cooling system", HT and LT cooling circuits are combined in sequence to one water circuit

In order to use the different temperature levels, the HT suction side is connected to the LT delivery side. The HT circuit uses an amount of warm LT water and further heats it up by cooling the engine. The amount of LT water, that is used by the HT system, depends on the current temperature and engine power. The overrun of the fixed flow of the fresh water pump (fitted on engine) HT (FP1) circulates via bypass line from the temperature control valve HT (FR1) to the suction side as usual.

The advantage of the secondary circuit system is it's simplicity. It uses just one water circuit and there is only one header tank and one fresh water cooler instead of two.

In addition also the amount of piping is reduced.

8.2 Water quality requirements

8.2.1 General

The engine cooling water must be carefully selected, treated and controlled.

The use of untreated cooling water will cause corrosion, erosion and cavitation on the surfaces of the cooling system. Deposits can impair the heat transfer and may result in thermal overload on components to be cooled

Therefore the treatment with an anti-corrosion agent has to be effected before the very first commissioning of the plant.

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8.2.2 Requirements

The characteristic of the untreated cooling water must be within the following limits:

- Distillate or freshwater free from foreign matter (no seawater or waste water)
- A total hardness of max. 10° dH
- pH-value 6.5 8
- Chloride ion content of max. 50 mg/l

8.2.3 Supplementary information

Distillate:

If a distillate or fully desalinated water is available, this should preferably be used as engine cooling water.

Hardness:

Water with more than 10° dGH (German total hardness) must be mixed with distillate or softened.

8.2.4 Treatment before operating the engine for the first time

Treatment with an anti-corrosion agent must be done before the engine is operated for the first time to prevent irreparable initial damage.

8.3 Recommendation for cooling water system

8.3.1 Pipes and tanks

Galvanized material should not be used in tanks and pipes, it can cause zinc attack in the engine.

8.3.2 Drain tank with filling pump

It is recommended to collect the treated water in a separate drain tank when carrying out maintenance work (to be installed by the yard).

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8.3.3 Electric motor driven pumps

Pumps should be applicable for use in fresh water as well as sea water circuits, vertical design.

Rough calculation of power demand for the electric balance:

$$p = \frac{\rho \cdot H \cdot V}{367 \cdot \eta} [kW]$$

P = Power [kW]

 $P_{M} = Power of electr. motor [kW]$

V = Flow rate [m³/h]

H = Delivery head [m]

 $\rho = Density [kg/dm^3]$

 η = Pump efficiency, 0.70 for centrifugal pumps

 $\begin{array}{lll} P_{M} = & 1.5 \cdot P & < 1.5 \, kW \\ P_{M} = & 1.25 \cdot P & 1.5 - 4 \, kW \\ P_{M} = & 1.2 \cdot P & 4 - 7.5 \, kW \\ P_{M} = & 1.15 \cdot P & 7.5 - 40 \, kW \\ P_{M} = & 1.1 \cdot P & > 40 \, kW \end{array}$

8.4 Cooling water system

General note: The following system diagrams should be regarded as typical examples. Their purpose is to explain the general function of the engine's systems. Numerous other variants and arrangements are possible and can be discussed and developed with the mechanical MaK A&I department.

8.4.1 General

The high temperature (HT) system provides the HT side of the charge air cooler and the engine's cylinder heads and cylinder liner water rings with cooling water. In order to reduce the thermal tension in water-cooled engine parts, it is important to keep the drop in temperature low and therefore the flow high. Therefore the fresh water pump (fitted on engine) HT (FP1) delivers its full flow over the engine.

The HT outlet temperature of 90 °C is controlled by the temperature control valve HT (FR1). In case the temperature decreases, the valve delivers more water to the bypass (connection B for mechanical, connection 3 for electrical driven valves) back to the HT pump's suction side.

In order to use the thermal energy of the HT circuit, a heat recovery can be installed as shown in the cooling water diagrams (FH3). For heat recoveries, especially for fresh water generators a high flow over the heat consumer (FH3) is recommended. This can be achieved by using a flow temperature control valve HT (FR3). This valve raises the HT flow temperature and therefore reduces the amount of water that is circulated over the bypass of FR1 and increases the flow through the heat recovery heat consumer (FH3) and the fresh water cooler HT (FH1).

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The low temperature (LT) cooling circuit provides cooling for the LT stage of the charge air cooler, the lube oil and the diesel oil coolers and possible other consumers like e.g. gear box and generator coolers. The LT flow temperature is controlled by FR2. The cooling system is laid out for 38 °C under tropical conditions and full engine load. For better performance, the LT temperature is to be controlled to 32 °C. Caterpillar Motoren can deliver mechanic P-controllers with a set point range of 20 to 30 °C or electric driven valves with electronic controllers, which must be set to 32 °C.

Depending on the plant design the HT fresh cooling water pump can be fitted on the engine or be supplied separate with an electrical drive.

Cooling water system diagram

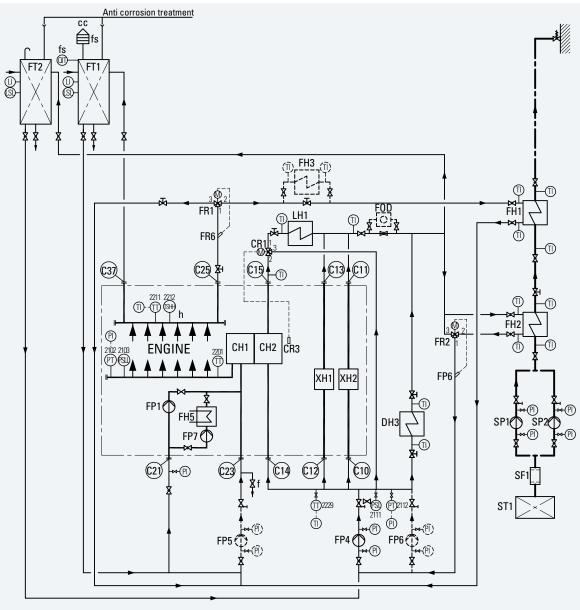


Fig. 8-1 Cooling water system diagram - Two circuit system

In plants with skin or box coolers not required: seawater system (SP1, SP2, SF1, ST1).

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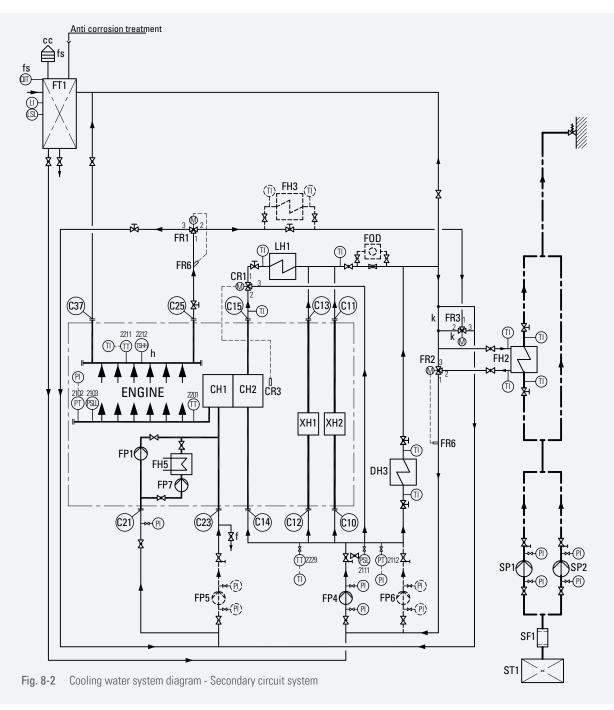
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CH1	Charge air cooler HT	FOD	Oil in water detector (optional)
CH2	Charge air cooler LT	LI	Level indicator
CR1	Charge air thermostat	LSL	Level switch low
DH3	Fuel oil cooler for MDO operation	PI	Pressure indicator
FH1	Fresh water cooler HT	PSL	Pressure switch low
FH2	Fresh water cooler LT	PSLL	Pressure switch low
FH3	Heat consumer	PT	Pressure transmitter
FH5	Fresh water preheater	QIT	Gas alarm and transmitter
FP1	Fresh water pump HT	TI	Temperature indicator
FP4	Fresh water pump (separate) LT	TSHH	Temperature switch high
FP5	Fresh water stand-by pump HT	TT	Temperature transmitter
FP6	Fresh water stand-by pump LT		
FP7	Preheating pump	C10	Connection, HT-controller,
FR1	Temperature control valve HT		generator bearing, inlet
FR2	Temperature control valve LT	C11	Generator bearing, outlet
FR6	Sensor for temperature control valve LT	C12	Generator cooler, inlet
FT1	Compensation tank HT	C13	Generator cooler, outlet
FT2	Compensation tank LT	C14	Charge air cooler LT, inlet
LH5	Oil cooler C.P. propeller	C15	Charge air cooler LT, outlet
SF1	Seawater filter	C21	Fresh water pump, inlet
SP1	Seawater pump	C23	Stand-by pump HT, inlet
SP2	Seawater stand-by pump	C25	Cooling water, engine outlet
ST1	Sea chest	C37	Vent
XH1	Generator cooler		
XH2	Generator bearing cooler	CC	Flame arrestor must be provided.
		f	Drain.
		h	Please refer to the measuring point list regarding design of the monitoring devices
		fs	Depending on classification society

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Cooling water system diagram – Secondary circuit



In plants with skin or box coolers not required: seawater system (SP1, SP2, SF1, ST1).

CH1	Charge air cooler HT	FOD	Oil in water detector (optional)
CH2	Charge air cooler LT	LI	Level indicator
CR1	Charge air thermostat	LSL	Level switch low
CR3	Sensor for charge air temperature control	PI	Pressure indicator
CHO	valve	PSL	Pressure switch low
DH3	Fuel oil cooler for MDO operation	PSLL	Pressure switch low
FH2	Fresh water cooler LT	PT	Pressure transmitter
FH3		QIT	Gas alarm and transmitter
	Heat consumer		
FH5	Fresh water preheater	TI	Temperature indicator
FOD	Oil water detector	TSHH	Temperature switch high
FP1	Fresh water pump HT	TT	Temperature transmitter
FP2	Fresh water pump (fitted on engine) LT		
FP7	Preheating pump	C10	Connection, HT-controller,
FR1	Temperature control valve HT		generator bearing, inlet
FR2	Temperature control valve LT	C11	Generator bearing, outlet
FR3	Flow temperature control valve HT	C12	Generator cooler, inlet
FR6	Sensor for temperature control valve LT	C13	Generator cooler, outlet
FT2	Compensation tank LT	C14	Charge air cooler LT, inlet
LH1	Lube oil cooler	C15	Charge air cooler LT, outlet
LH3	Gear lube oil cooler	C21	Fresh water pump, inlet
SF1	Seawater filter	C23	Stand-by pump HT, inlet
SP1	Seawater pump	C25	Cooling water, engine outlet
SP2	Seawater stand-by pump	C37	Vent
ST1	Sea chest		
XH1	Generator cooler	CC	Flame arrestor must be provided.
XH2	Generator bearing cooler	f	Drain.
		h	Please refer to the measuring point list
			regarding design of the monitoring devices.
		fs	Depending on classification society.
		k	Distance min. 1 m.

8.4.2 Components

Freshwater cooler LT FH2 (separate)

Plate type, size depending on the total heat to be dissipated.

Most ship cooling systems dump the engines' waste heat in seawater cooled fresh water coolers.

Caterpillar Motoren offers standardized titanium plate heat exchangers for this purpose.

The size of these coolers will always be individually calculated for the heat dissipation demand of the respective systems.

Alternatively box coolers, radiators and other heat exchanger arrangements and any kind of combined cooling systems can be laid out and delivered.

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Compensation tank HT FT1 / LT FT2

- Arrangement: Min. 4 / max. 16 m above crankshaft center line (CL).
- Size according to technical engine data.
- All continuous vents from engine are to be connected.

Main functions of the cooling water header tank:

- It produces static pressure for the cooling water pumps in order to prevent cavitation. Therefore it
 has to be connected to each pump suction side or in case of a combined system to the suction side of
 the central cooling water pump.
- The vent lines continuously deliver a small water flow to the header tank. In this flow, air bubbles are carried away and the system gets de-aerated.
 - Vent lines should also be installed in the highest points of the circuits in order to get rid of all air bubbles that accumulate there.
 - Vent lines may not be too large in order to keep the flow over the header tank low. DN 20 is recommended and also valves for adjusting the flow must be installed.
- The flow of the vent lines gradually heats up the header tank by means of the constantly delivered
 hot water. This flow returns to the system via the pump suction side. As this circulation is very small
 in relation to the flow of the pump (if adjusted correctly), the temperature rise in the system will not be
 noticeable.
- The header tanks water volume balances the entire system volume, which changes due to thermal expansion and possibly due to leakages.

NOTE: Some marine classification societies require the HT compensation tank to be equipped with a gas sensor.

Electric driven charge air temperature control valve CR1 (separate)

		Dimensions [mm]					
	DN	А	В	С	D	[kg]	
6/7 M 46 DF	100	350	646	175	170	70	
8/9 M 46 DF	125	400	717	200	170	110	
_	150	480	742	240	170	149	

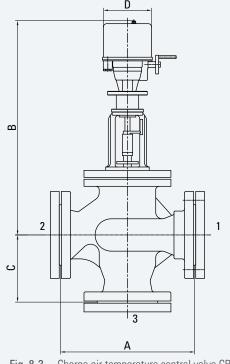


Fig. 8-3 Charge air temperature control valve CR1

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Fresh water pump (separate) HT FP3/FP5 and LT FP4/FP6

Capacity: acc. to heat balance.

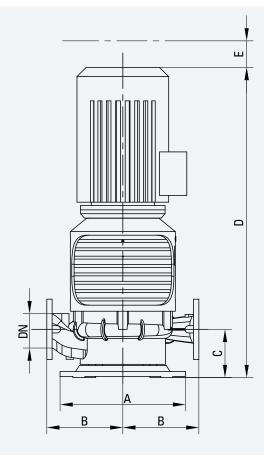


Fig. 8-4 Fresh water pump

Flow	Pressure	Dimensions [mm]							
[m³/h]	[bar]	DN	А	В	С	D	Е	[kg]	
70	3	80	460	260/200	158	913	110	130	
100	3	125	510	285/225	183	889	110	180	
140	3	150	510	285/225	183	889	110	182	
180	3	150	735	380/355	251.5	1,082.5	110	330	

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Temperature control valve HT FR1 / LT FR2 / HT flow FR3

P-controller with manual emergency adjustment (basis).

Option: PI-controller with electric drive. See charge air temperature control valve (CR1).

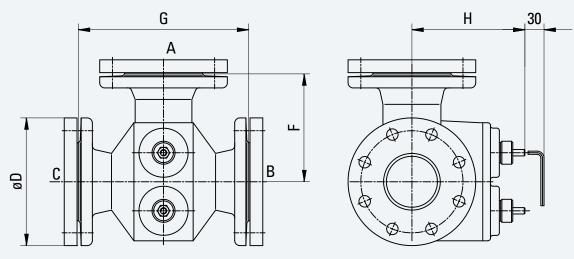


Fig. 8-5 Temperature control valve HT FR1

			Dimensions [mm]						
		DN	D	F	G	Н	[kg]		
6/7 M 46 DF	HT	125	250	241	489	200	67		
8/9 M 46 DF	HT	150	285	254	489	200	80		
6/7/8/9 M 46 DF	LT	150*)	285	254	489	200	80		

^{*)} Minimum depending on total cooling water flow

8.5 System diagrams heat balance

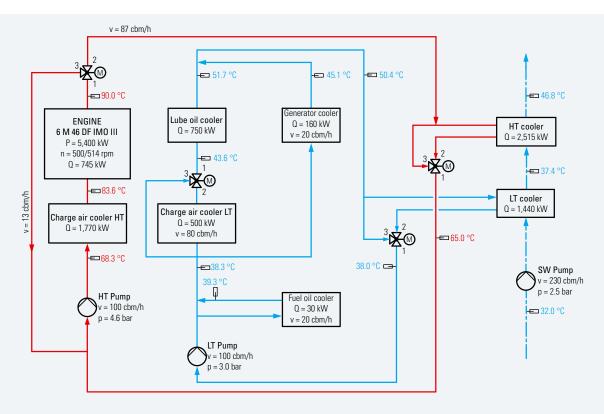


Fig. 8-6 Heat balance, system diagram 6 M 46 DF, 900 kW/Cyl.

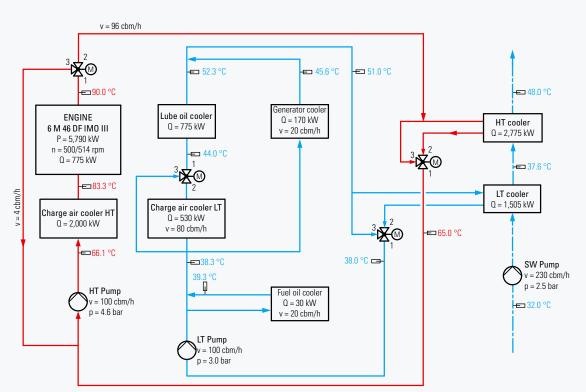


Fig. 8-7 Heat balance, system diagram 6 M 46 DF, 965 kW/Cyl.

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v = 84 cbm/h 3 X (W) **=** 54.0 °C **←** 46.4 °C **-**□ 52.5 °C **-**□ 46.7 °C **=**90.0 °C enerator coole Lube oil cooler **ENGINE** Q = 190 kWHT cooler 7 M 46 DF IMO III Q = 875 kWv = 20 cbm/hQ = 2,935 kWP = 6,300 kWn = 500/514 rpm**←** 44.6 °C ³12 00 Q = 870 kW**─** 37.4°C ³₩<u></u>₩ -**=**33.2 °C LT cooler v = 26 cbm/hQ = 1,680 kW Charge air cooler LT Charge air cooler HT Q = 585 kW Q = 2,065 kWv = 80 cbm/h³| | | | | | | | -**□** 60.0 °C € 67.0 °C 38.0 °C **□ -**■38.3 °C SW Pump v = 270 cbm/h 39.3 °C ☐ p = 2.5 bar HT Pump Fuel oil cooler v = 110 cbm/h 0 = 30 kW**=** 32.0 °C p = 4.5 bar v = 20 cbm/hLT Pump v = 100 cbm/hp = 3.0 bar

Fig. 8-8 Heat balance, system diagram 7 M 46 DF, 900 kW/Cyl.

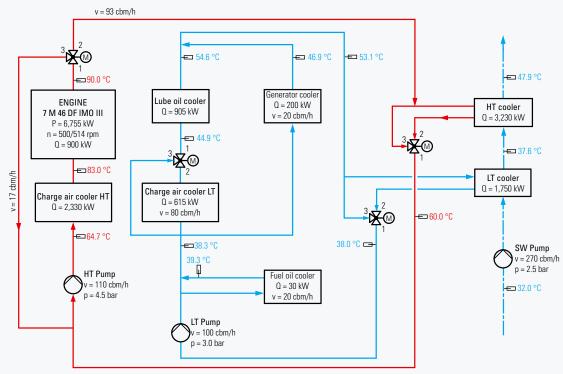


Fig. 8-9 Heat balance, system diagram 7 M 46 DF, 965 kW/Cyl.

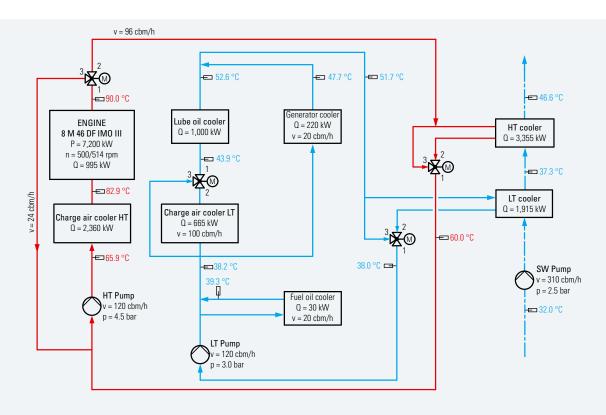


Fig. 8-10 Heat balance, system diagram 8 M 46 DF, 900 kW/Cyl.

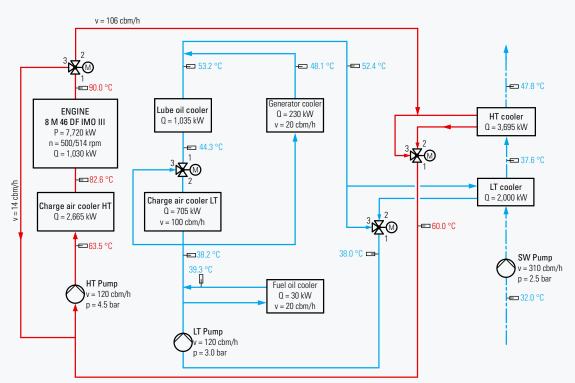


Fig. 8-11 Heat balance, system diagram 8 M 46 DF, 965 kW/Cyl.

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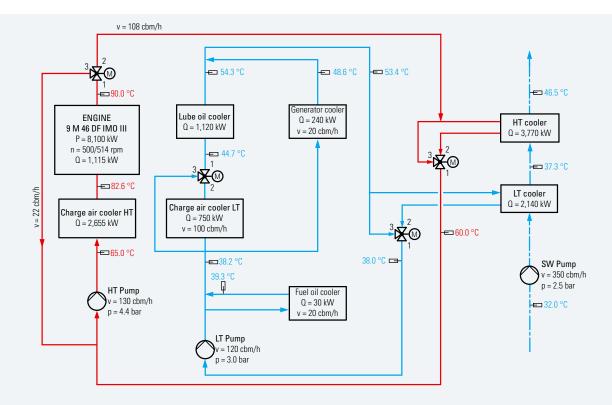


Fig. 8-12 Heat balance, system diagram 9 M 46 DF, 900 kW/Cyl.

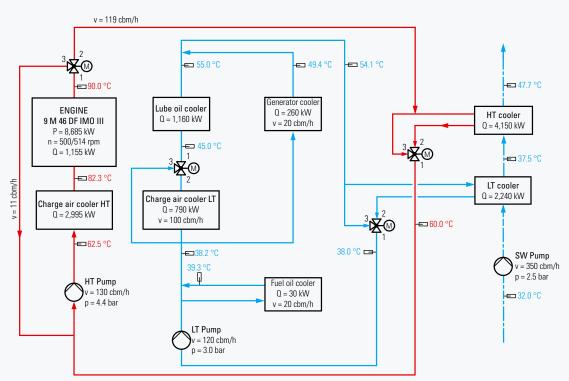


Fig. 8-13 Heat balance, system diagram 9 M 46 DF, 965 kW/Cyl.

COOLING WATER SYSTEM

8.6 Preheating (separate module)

8.6.1 Electrically heated

- The standard preheating system in plants delivered by Caterpillar Motoren is electrically heated.
- Consisting of baseframe mounted preheating pump FP7 (12 m³/h), electric heater FH5 (48 kW) and separate switch cabinet.

Voltage 400 - 690, frequency 50/60 Hz.

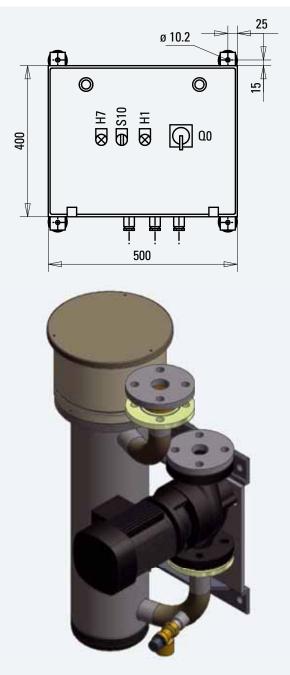


Fig. 8-14 Freshwater preheater FH5, preheating pump FP7

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COOLING WATER SYSTEM

8.6.2 Other preheating systems

On request preheating systems heated by thermal oil or steam can be laid out and delivered by Caterpillar Motoren.

8.7 Box coolers system

On request box coolers can be laid out and delivered by Caterpillar Motoren.

8.8 Cooling circuit layout

The engine driven cooling water pumps are designed to provide the engine and it's systems with cooling water.

For a rough layout of these circuits, a pressure drop of 0.5 bar per component can be calculated: Taking the total estimated pressure loss of the whole circuit in account, the flow delivered by the pump can be read out from the pump performance curve.

Engine driven cooling water pumps Performance curve

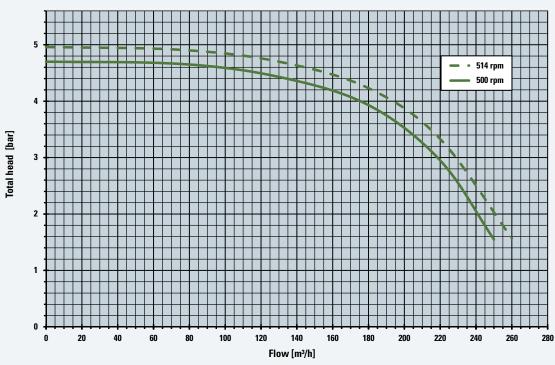


Fig. 8-15 Pump curve

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9.1 General

M 46 DF engines require compressed air for starting the engine and providing actuating energy for safety and control devices as well as for Flexible Camshaft Technology (FCT).

The compressed air system consists at least of two compressors, two air receivers and its accessories such as filters, dryers, regulating and control valves and the piping system, of a capacity and air delivery rating dependent of the load profile of the ship and to meet the requirements of the respective classification society.

To ensure always the functionality of the compressed air system, it has to be free of solid particles and oil, see chapter 9.4 Compressed air quality.

9.2 Internal compressed air system

The M 46 DF engine is started by means of compressed air with a nominal pressure of 30 bar.

The start is performed by direct injection of starting air into the cylinder through the starting air valves in the cylinder heads.

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9.3 Compressed air system

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Clean and dry starting air is required. A starting air filter has to be installed before engine, if required. Module P&ID's must be considered for detailed description.

Caterpillar Motoren recommends installing automatic drain valves.

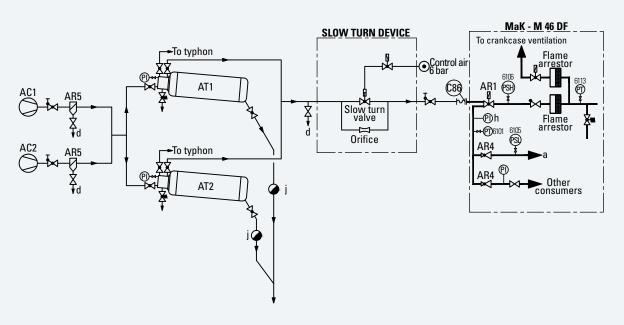


Fig. 9-1 External compressed air system, system diagram

AC1 AC2 AR1 AR4 AR5 AT1 AT2	Compressor Stand-by compressor Starting valve Pressure reducing valve Oil and water separator Starting air receiver (air bottle) Starting air receiver (air bottle)
PI PSH PSL PT	Pressure indicator Pressure switch high Pressure switch low, only for main engine Pressure transmitter Connection / starting air

а	Control air
d	Water drain (to be mounted at the lowest
	point)
h	Please refer to the measuring point list
	regarding design
j	Automatic drain required
AT1/AT2	2 Option:
	- Typhon valve
	- Relief valve with pipe connection

9.3.1 Compressor AC1 / AC2

According to the requirements of the Marine Classification Society there should be minimum 2 starting air compressors with 50% total performance each.

The total performance has to be sufficient for refilling the starting air receivers to their normal pressure of 30 bar within one hour.

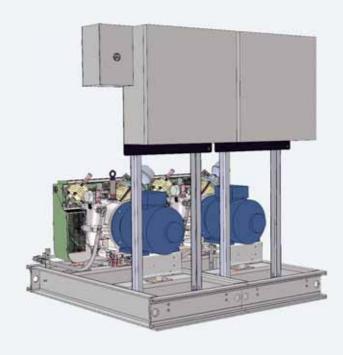


Fig. 9-2 Compressor AC1, AC2

Capacity:

 $V [m^3/h] = \sum_{Rec.} V_{Rec.} \cdot 30$

V_{Rec.} Total receiver volume [m³]

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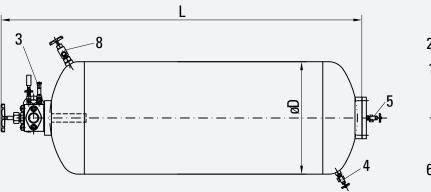
9.3.2 Air receiver AT1 / AT2

The starting air receivers are to be dimensioned for a nominal pressure of 30 bar.

M 46 DF engines require at least 14 bar as a minimum starting air pressure.

The total amount of air receivers and their capacity depend on the requirements of the classification societies and the type of installation.

It is required to install the receivers in a way, so that it can always sufficiently be drained manually or automatically at the deepest point of the receivers.



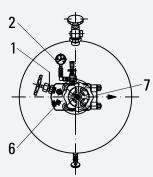


Fig. 9-3 Air receiver AT1, AT2

- 1 Filling valve
- 2 Pressure gauge G 1/4
- **3*** Relief valve DN 7
- 4 Drain valve DN 8
- 5 Drain position vertical

- 6 Connection G 1/2 with plug
- 7 Outlet of starting valve at engine
- 8 Typhon valve DN 16

Option: * with pipe connection G 1/2

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Normal requirements of classification societies:

No. of starts: 6 + 1 Slow turn

No. of receivers: min. 2

Calculation of air receiver volumes:

$$V = \frac{V_2 \cdot n \cdot P_{atm}}{P_{max} - P_{min}}$$

V = Air receiver volume

 V_2 = Air consumption per start [Nm³]

n = Required number of starting procedures in sequence

P_{atm} = Ambient pressure [bar]

 P_{max} = Maximum receiver pressure (30 bar) P_{min} = Minimum receiver pressure (14 bar)

Receiver capacity acc. to GL recommendation AT1/AT2

	Single-engine plant	Twin-engine plant
6/7 M 46 DF	2 x 750 l	2 x 1,500 l
8/9 M 46 DF	2 x 1,000 l	2 x 2,000 l

Receiver capacity	L	øD	Valve head	Weight
[1]	[mm]	[mm]		approx. [kg]
250	2,037	480	DN 38	280
500	3,501	480	DN 50	460
750	3,033	650	DN 50	625
1,000	3,853	650	DN 50	810
1,500	3,753	800	DN 50	1,150
2,000	4,903	800	DN 50	1,490

When CO₂ fire extinguishing plants are arranged in the engine room, the blow-off connection of the safety valve is to be piped to the outside.

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9.4 Compressed air quality

For a proper operation of the engine a compressed air quality of class 4 according ISO 8573-1 is required.

Instrument air specification

Max. particle size: 15 μ m Max. particle density: 8 mg/m^3 Water pressure dew point: 3 °C

Water: 6.000 mg/m³
Residual oil content: 5 mg/m³

• Oil content

(Specification of aerosols and hydrocarbons which may be contained in the compressed air.)

Particle size and density

(Specification of size and concentration of particles which still may be contained in the compressed air.)

Pressure dew point

(Specification of the temperature on which the compressed air can cool down without the steam contained in it condensing. The pressure dew point changes with the air pressure.)

9.5 Slow turn

A slow turning device is mandatory and has to be installed, one per engine.

This is a precaution in case a cylinder has had oil or water leak into it, which would cause damage to the engine when starting.

If the engine completes two full revolutions on slow turn, the automatic main starting air will open for starting the engine.

	6 M 46 DF	7 M 46 DF	8 M 46 DF	9 M 46 DF
Air consumption per slow turn manoeuvre [Nm³]	5.2	5.4	6.4	6.6

9.6 Equipment

Compressor module

Caterpillar Motoren can design, offer and deliver integrated compressor modules: Starting air receiver and compressors can be combined individually.

For further information please contact Caterpillar Motoren, technical department.



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COMBUSTION AIR SYSTEM

10.1 Engine room ventilation

To obtain good working conditions in the engine room and to ensure a trouble free operation of all equipment a properly designed engine room ventilation system with cooling air and combustion air is required.

10.2 Combustion air system design

Combustion air describes the air the engine requires to burn fuel. Combustion air demand see chapter 4, technical data.

10.2.1 Air intake from engine room (standard)

- Fans are to be designed for a slight overpressure in the engine room.
- On system side the penetration of water, sand, dust, and exhaust gas must be avoided.
- When operating under tropical conditions, the air flow must be conveyed directly to the turbocharger.

10.2.2 Air intake from outside

- The intake air duct is to be provided with a filter. Penetration of water, sand, dust and exhaust gas must be avoided.
- Connection to the turbocharger is to be established via an expansion joint.
 For this purpose the turbocharger will be equipped with a connection socket.

10.2.3 Air intake temperature from engine room and from outside

- Standard engine operation is possible with an air temperature at the turbocharger inlet above 0 °C.
- Engine operation below 0 °C requires an ignition pressure reduction via waste gate interaction (standard scope of supply) which could occur in a load reduction and / or in higher fuel consumption.

10.3 Cooling air

Cooling air refers to the flow of air that removes radiant heat from the engine, generator, other driven equipment and other engine room components.

To dissipate the radiated heat a slight and evenly distributed air flow is to be led along the engine exhaust gas manifold starting from the turbocharger.

NOTE:

Radiated heat see technical data.

10.4 Condensed water from charge air duct

Operating the engine in tropical conditions, high ambient temperature and high humidity, may generate condensate (water) that needs to be drained.

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The exhaust gas system discharges the exhaust gases, emitted from the engine, through a piping system to the atmosphere. To provide maximum efficiency of the engine, the resistance to the gas flow should be minimized. The back pressure directly after the turbocharger, influenced by the design of the exhaust gas piping and all installed components like exhaust gas boilers, catalysts and scrubbers is limited to 30 mbar. Higher values will increase the thermal load of the engine and may lead to higher fuel consumption.

11.1 Components

11.1.1 Exhaust gas nozzle

For an optimal integration of the engine in the engine room, regarding the discharge of the emitted exhaust gases different orientations of the exhaust gas nozzle are possible.

The basic orientation of the exhaust gas nozzle for all M 46 DF engines is 45 $^{\circ}.$

Transition pieces are available also for orientations of 0 $^{\circ}$, 30 $^{\circ}$, 60 $^{\circ}$ and 90 $^{\circ}$ from the vertical line.

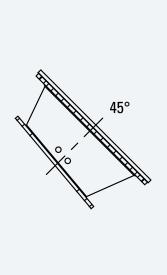


Fig. 11.1 Basic orientation

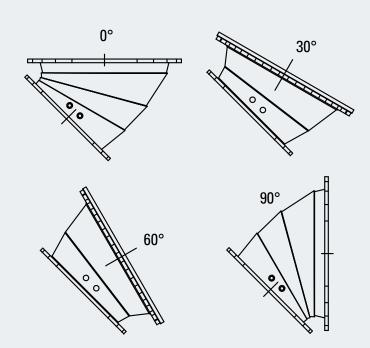


Fig. 11-2 Orientations with transition pieces

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11.1.2 Exhaust gas compensator

The connection of the engine to the piping system of the ship has to be flexible to compensate possible engine vibrations, movements of resilient mounted engines and to reduce the forces generated by the thermal expansion of the exhaust gas piping acting to the turbocharger. For this connection a special type approved exhaust gas compensator which is flexible in all directions is available.

It is highly recommended to install the exhaust gas compensator directly after the above mentioned

It is highly recommended to install the exhaust gas compensator directly after the above mentioned exhaust gas nozzle. If it is necessary to isolate the compensator area it must be possible that the compensator is able to expand and contract freely.

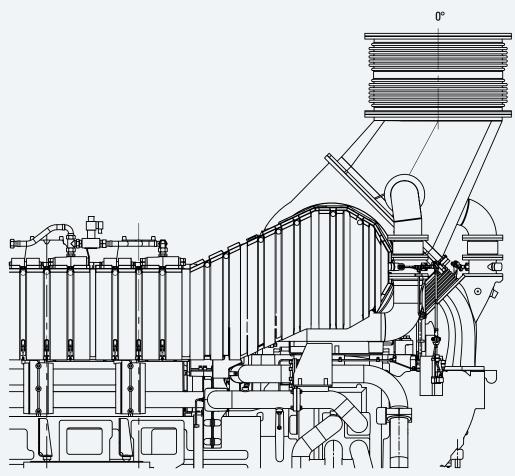


Fig. 11-3 Exhaust gas compensator

Basic design values of the standard exhaust gas compensators.

Typo	Diameter	Length	Weight	
Туре	[mm]	[mm]	[kg]	
6 M 46 DF	900	500	158	
7/8/9 M 46 DF	1,000	620	209	



11.1.3 Exhaust gas piping system

To minimize the forces acting through the compensator to the turbocharger and to guarantee a long lifetime of the compensator it is highly recommended to position a fixed point piping support directly after the compensator.

Each engine requires a separate exhaust gas pipe. The exhaust gas piping system of two or more engines is not allowed, otherwise exhaust gases from engines under operation be forced into cold engines not operating and causes engine damages as a result of condensed water from the exhaust gas.

Also the exhaust gas pipes and/or silencers should be equipped with water separating pockets and a drainage.

In order to minimize the pressure loss of the complete exhaust gas system it is recommended to use a suitable pipe diameter for the entire exhaust gas line.

According to the dimensions of the compensators (see table chapter 11.1.2) there are standard diameters proposed for the respective engine type in relation to the exhaust gas mass flow. In case of multiple of bends and other components integrated in the exhaust gas system it might be necessary to increase the pipe diameter.

For guidance the exhaust gas flow velocity should be less than 40 m/s.

For flushing the exhaust gas piping system after engine operation in gas mode an installation of a forced ventilation system is required.

According to class requirements explosion relief valves for single main engines and for multi-engine installations at least burst discs for explosion release device has to be installed in the exhaust gas system. For each individual installation the number and size of these devices will be determined by a simulation.

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Resistance in exhaust gas piping

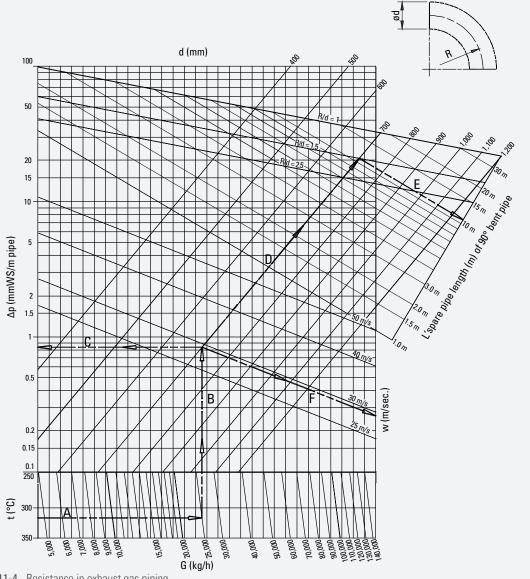


Fig. 11-4 Resistance in exhaust gas piping

Example (based on diagram data A to E):

 $T = 335 \,^{\circ}\text{C}, G = 25,000 \,\text{kg/h}$

L = 15 m straight pipe length, d = 700 mm

3 off 90 $^{\circ}$ bend R/d = 1.5

1 off 45 $^{\circ}$ bend R/d = 1.5

 $\Delta Pg = ?$

 $\Delta p = 0.83 \text{ mm WC/m}$

 $L' = 3 \cdot 11 \text{ m} + 5.5 \text{ m}$

L = I + L' = 15 m + 38.5 m = 53.5 m

 $\Delta Pg = \Delta p \cdot L = 0.83$ mm WC/m - 53.5 m = 44.4 mm WC

t = Exhaust gas temperature [°C]

G = Exhaust gas massflow [kg/h]

 $\Delta p = Resistance/m pipe length [mm WC/m]$

d = Inner pipe diameter [mm]

w = Gas velocity [m/s]

I = Straight pipe length [m]

L' = Spare pipe length of 90 ° bent pipe [m]

L = Effective substitute pipe length [m]

 Δ Pg = Total resistance [mmWC]

11.1.4 Silencer

The exhaust noise emission of the engine has to be reduced by an integration of at least one suitable silencer in the exhaust gas system to fulfil either the specifications of the relating classification company or legal regulations according to noise emissions or just to meet the clients comfort demand at open deck. Standard silencers which are especially designed for each engine type are available. As the silencers are of the absorptive type the flow resistance is low so just a back pressure of approximately 100 mmWC will arise. Long fibre absorbing heat resistant material is used for the noise absorption.

The noise attenuation of the standard silencers reaches at least 35 dB(A) and covers a wide frequency range. If necessary also silencers with a higher attenuation can be offered.

As standard the silencer can be provided either with or without a spark arrestor which will be provided with a soot collecting chamber. Each silencer is equipped with a water drain to draw out the condensed water. The silencer will be delivered with counter flanges, screws and gaskets. The mounting brackets for either horizontal or vertical installation as the insulation are not included. Optional the silencers can be delivered with loose or welded on mounting brackets according clients requirements.

Special attention has to be paid to the positioning of the silencer in the exhaust gas system to avoid resonance effects in the piping system. A wrong positioning of the silencer in the system can cause high noise levels before or after the silencer and can lead to extreme noise at the funnel end.

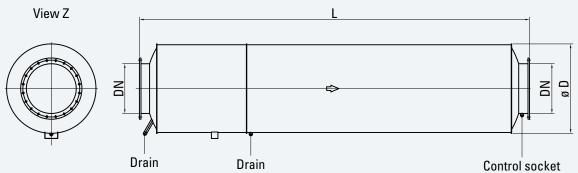
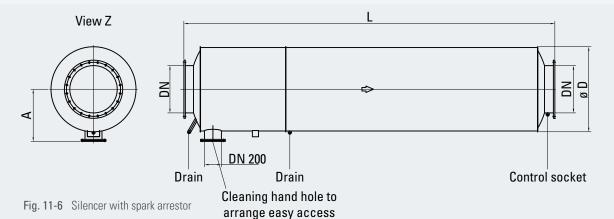


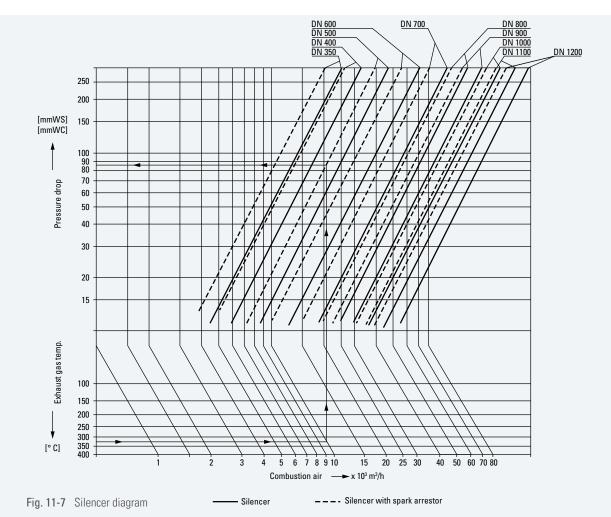
Fig. 11-5 Silencer



Tuno	Dimensions [mm]				Weight	Weight with spark arrestor
Туре	DN	А	D	L	[kg]	[kg]
6 M 46 DF	900	1,110	1,700	6,150	3,400	2,950
7/8/9 M 46 DF	1,000	1160	1,800	6,460	3,900	3,540

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Exhaust gas boiler

11.1.5

If exhaust gas boilers are used in the exhaust gas line each engine should have a separate boiler. If a common boiler is used for two or more engines the gas sections have to be separated.

Particularly when exhaust gas boilers are installed attention must be paid not to exceed the maximum

11.2 Turbocharger

recommended back pressure.

11.2.1 Turbine cleaning system

Turbine cleaning is required for HFO operation. The cleaning is carried out with clean fresh water "wet cleaning" during low load operation at regular intervals, depending on the fuel quality, 150 hours.

NOTE:

Duration of the cleaning period is approx. 15 minutes (2 intervals). Fresh water of 2 - 2.5 bar is required.

NOTE:

During cleaning the water drain should be checked. Therefore, the shipyard has to install a funnel after connection point C36.

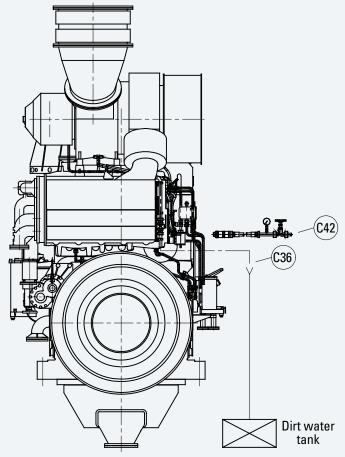


Fig. 11-8 Connection points fresh water and drain

C42 Fresh water supply, DN 12C36 Drain, DN 30

Typo	Water flow	Injection time		
Type	[l/min]	[min]		
6 M 46 DF	23 - 27	10		
7/8/9 M 46 DF	32 - 38	10		

11.2.2 Compressor cleaning system

The components for cleaning (dosing vessel, pipes, shut-off valve) are engine mounted.

NOTE:

Water is fed every 24 hours before compressor wheel via injection pipes during full load operation.

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FLEXIBLE CAMSHAFT TECHNOLOGY (FCT)

12.1 Flexible Camshaft Technology (FCT)

The dual fuel engine has a modified FCT system, to ensure an optimal engine operation in all operating modes over the entire load range. The FCT system is basically known from the M 32 C diesel engine, where this technology is already validated.

Benefits:

- High potential for smoke reduction
- Low complexity
- Low technical risk-application of existing technology
- Increase knock margin at higher engine loads

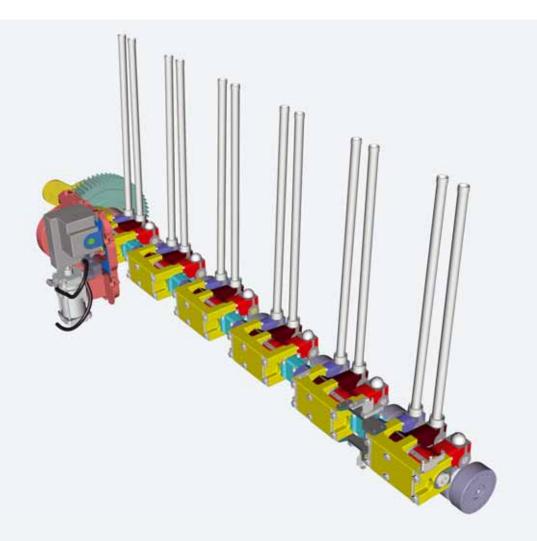


Fig. 12-1 Valve train with Flexible Camshaft Technology

13.1 Local control panel (LCP)

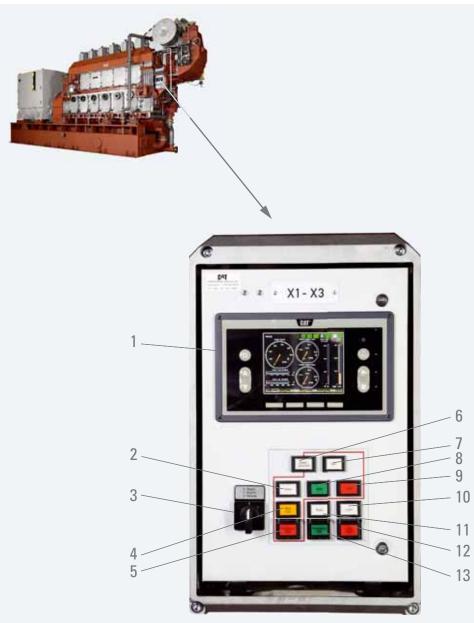
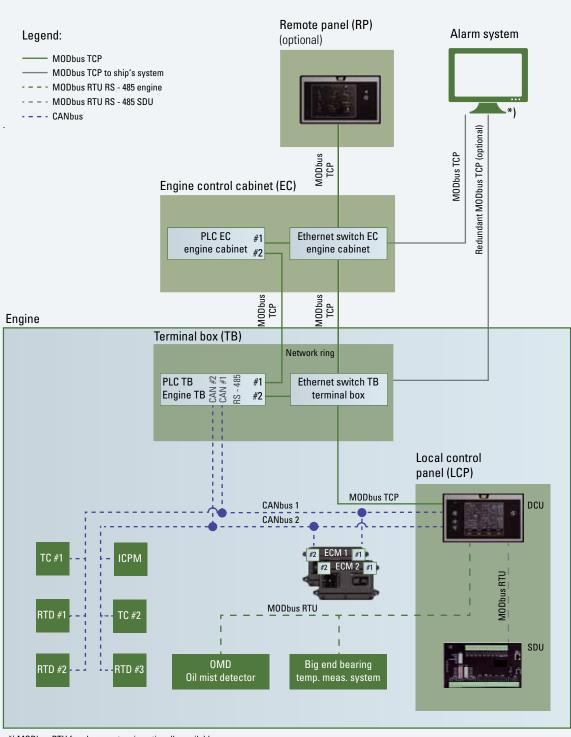


Fig. 13-1 Local control panel

1	DCU (Display and alarm system)	8	Start
2	Reset	9	Stop
3	0 = Repair, 1 = Engine, 2 = Remote	10	Lower
4	Slow turn	11	Raise
5	Emergency stop	12	Gas shut-off
6	Diesel mode indication, lamp test	13	Emergency start
7	Gas mode indication		

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13.2 Data link overview



*) MODbus RTU for alarm system in optionally available

Fig. 13-2 Data link overview - M 46 DF

SDU

Protection system in local control panel

DCU

Display and alarm system in local control panel

PLC

PLC in engine cabinet (EC)

PLC in engine terminal box on engine (TB)

RTD

PT100 module for charge air temperature, lube oil temperature, cooling water HT/LT temperature and main bearing temperature

TC

Thermocouple modules for exhaust gas temperature

RP

Remote panel (optional)

External display for engine alarm and monitoring system

ECM

Engine control module

OMD

The oil mist detector measures each cylinder.

CTM

Big end bearing temperature monitoring

Each cylinder compartment of the cylinder crankcase is measured by the CTM.

ICPM

The "In-cylinder pressure monitoring" computes combustion characteristics for each cylinder including knock intensity per cylinder

Regardless of RTU or TCP, the MODbus address registers are the same. Just the hardware protocol differs.

MODbus TCP

At MODbus TCP a connection between server and client will be established. Therefore an IP address will be assigned.

MODbus settings

Type: MODbus TCP Interface: ethernet IP: will be assigned

Baud rate: 10 mbit/s / 100 mbit/s

Connector: RJ45

MACS

Modular Alarm Control System

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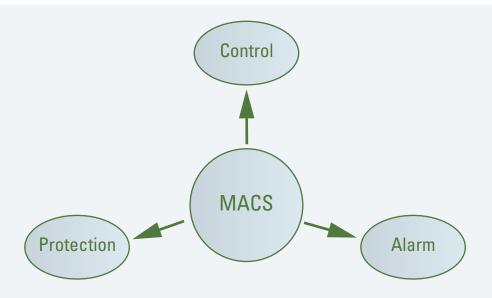
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13.3 Components

Modular Alarm and Control System (MACS)



The M 46 DF engines will be provided with a new Modular Alarm and Control System, called MACS. The basic engine control and monitoring system will be installed in the local control panel. Where extension modules are necessary external plc based I/O extension modules will be installed.

The main functions of the control systems are:

- Alarm management
- Local start and stop, emergency start and stop from the engine control panel
- Remote start and stop from the power management system (PMS)
- Start and stop sequence control
- Critical parameter monitoring
- Slow turn control
- Flexible camshaft technology (FCT monitoring)
- Exhaust gas termperature monitoring
- Main and big end bearings temperature monitoring

For the following modules the control and monitoring is integrated in MACS:

- Ignition fuel module
- Ventilation module
- Crankcase gas detection

Engine control module (ECM)

The engine control module controls the fuel system, air fuel ratio, engine speed and Flexible Camshaft Technology (FCT). The module has its own set of sensors for all control relevant functions and can operate independently from start/stop system, alarm system (DCU) or protection system (SDU). For multiple engine operation the ECM provides also load sharing functions. An isochronous load distribution by master/slave principle or droop operation is possible.

Oil mist detector (OMD)

The oil mist detector measures the oil mist concentration for each cylinder compartment and generate an alarm for high oil mist concentration. The data is available by MODbus RTU at the DCU. Hardwired outputs are also provided.

Big end bearing temperature measuring system (CTM)

The big end bearing temperature measuring system measures the temperature for each big end bearing and generates an alarm for high temperature. The data is available by MODbus RTU at the DCU. Hardwired outputs are also provided.

Gas valve unit (GVU)

The gas valve unit provides the engine with the desired gas fuel pressure and is controlled by the engine's control and monitoring system (MACS). It has several features (e.g. double block and bleed valve) to safety cut the engine from the gas train and to remove the gas fuel from the piping system (flushing).

Crankcase gas detection (CGD)

The crankcase gas detection system monitors the actual concentration of explosive atmosphere in the crankcase in means of methane concentration in lower explosion limit (LEL). If the concentration increases above a fixed value an alarm is triggered and in a second step the engine switches back to diesel mode.

Ventilation module (VM)

The aim of the ventilation module is to detect a leakage in the double walled gas pipes downstream the gas valve unit all the way over the engine. The air in the double walled gas pipe will be ventilated and the gas concentration will be measured.

Ignition fuel module (IFM)

The ignition fuel control system provides the required ignition fuel oil quality for the engine's ignition system.

Exhaust gas module (EGV)

The exhaust gas module is installed to ventilate the ship side exhaust gas system after an emergency stop of the engine in gas operation. The module consists of a ventilation fan, a separation butterfly valve and exhaust gas compensator for the connection to the exhaust gas system.

Slow turn device (STD)

The slow turn function is used to detect water in the combustion chamber, e.g. after a long non-operation period.

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13.4 Genset control

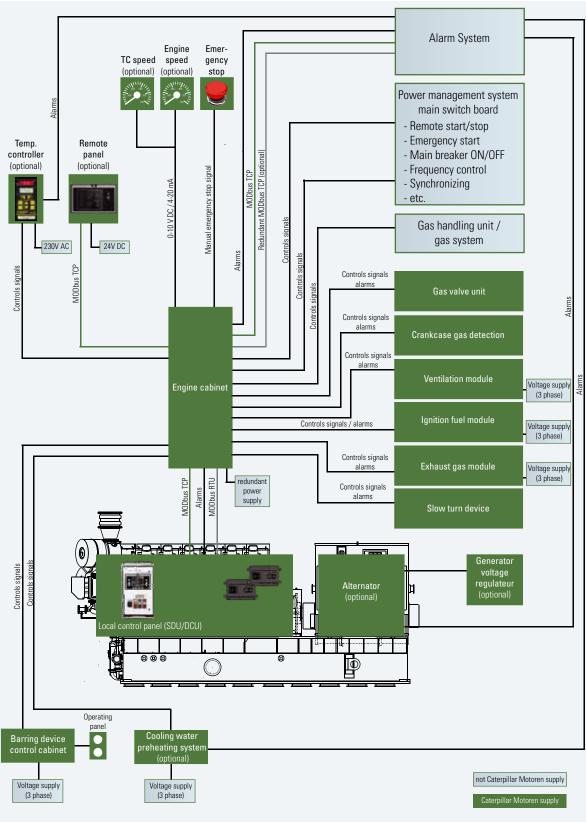


Fig. 13-3 Generator set control M 46 DF

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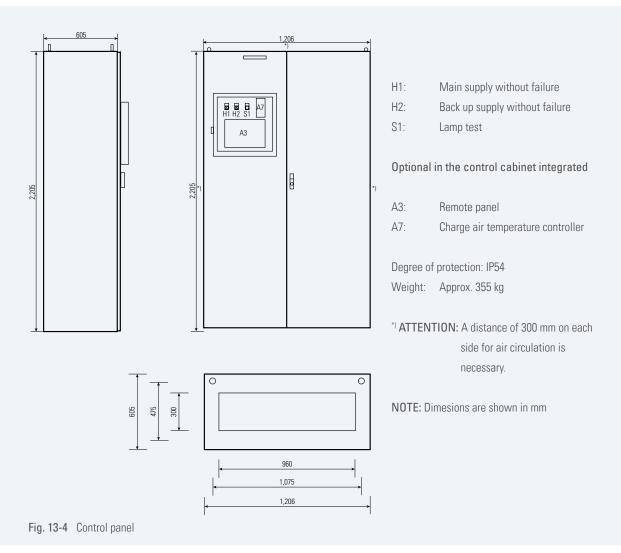
CONTROL AND MONITORING SYSTEM

13.5 Control cabinet

Each engine is equipped with a separate control cabinet. The control cabinet acts as an interface between engine and external devices. Information about the engine status are available via MODbus TCP or MODbus RTU (optionally).

External signals for the engine control, monitoring and alarm system (for example power management system, main switch board, gas system,...) can be transferred as 4-20 mA, binary, or PT100 signals. Safety relevant signals to the PLC are wire break and short circuit monitored.

The remote panel or the temperature controller can be optionally integrated in the control cabinet.



13.6 Requirements

13.6.1 Requirements on power management system

Standard interface to power management system / main switch board

Standard interface to power management system / main switch board								
	External starting interlock	Binary contact	\rightarrow	24 V DC	External starting interlock			
	External engine shutdown	Binary contact	\rightarrow	24 V DC	External engine shutdown			
	Blackout	Binary contact	\rightarrow	24 V DC	Blackout (start release of starting interlock prelubrication)			
	Indication shutdown undelayed/delayed	24 V DC	—	Binary contact	Shutdown undelayed/delayed			
	Load signal from kW transducer *)	4-20 mA	\rightarrow	Max. load 250 Ω	Load signal from kW transducer			
	Raise / Iower (remote)	Binary contact	\rightarrow	24 V DC	Raise / Iower (remote)			
	Isochronous / droop *)	Binary contact	\rightarrow	24 V DC	Isochronous / droop			
board	Status circuit breaker	Binary contact	\rightarrow	24 V DC	Circuit breaker closed (on for closed)			
witch	Bus tie signal	Binary contact	\rightarrow	24 V DC	Bus tie is closed			
main sv	Manual activation slow turn	Binary contact	\rightarrow	24 V DC	Slow turn mode change			
Power management system / main switch board	Automatic slow turn	Binary contact	\rightarrow	24 V DC	Slow turn selected for automatic	Main engine		
ent sys	Start/stop remote	Binary contact	\rightarrow	24 V DC	Start/stop in remote mode	Main		
ınagem	Change genset	24 V DC	—	Binary contact	Engine fault - change genset			
er ma	Normal stop indication	24 V DC	—	Binary contact	Normal stop indication			
Powe	Start initiation indication	24 V DC	←	Binary contact	Start initiation indication			
	Starting interlock indication	24 V DC	—	Binary contact	Starting interlock indication			
	Remote control active	24 V DC	—	Binary contact	Remote control active			
	Ready to start, indication	24 V DC	←	Binary contact	Ready to start, indication			
	False start indication	24 V DC	—	Binary contact	False start indication			
	rpm contact	24 V DC	—	Binary contact	rpm contact			
	Offload *)	Binary contact	\rightarrow	24 V DC	Offload			
	Isochronous selected *)	24 V DC	—	Binary contact	Isochronous selected			
	Emergency stop from PMS	Binary contact	\rightarrow	24 V DC	External emergency stop (from PMS)			

^{*)} For optionally isochronous load sharing.

13.6.2 Requirements on gas system

The table below shows the standard interface between the gas system and the dual fuel engine.

Standard interface to the gas system

	Indication diesel mode	24 V DC	—	binary	
	Indication gas mode	24 V DC	—	binary	
	Activate gas supply to gas valve unit	24 V DC	—	binary	
	Switch over to gas operation failed	24 V DC	—	binary	
	Gas operation shut off machinery space	24 V DC	—	binary	
m	Gas operation shut off engine	24 V DC	—	binary	inet
system	Gas mode interlock	24 V DC	—	binary	Engine cabinet
Gas	Gas operation shut down	binary	\rightarrow	24 V DC	Engin
	Gas mode interlock	binary	\rightarrow	24 V DC	
	Diesel mode select	binary	\rightarrow	24 V DC	
	Gas mode select	binary	\rightarrow	24 V DC	
	Inert gas supply pressure	4-20 mA	\rightarrow	Analogue output	
	Pressure transmitter fuel gas supply to engine room	4-20 mA	\rightarrow	Analogue output	

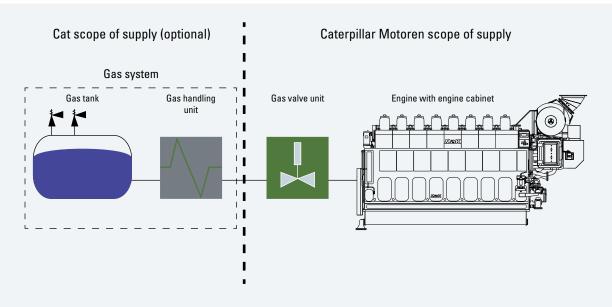


Fig. 13-5 Basic overview: dual fuel engine gas system

13.6.3 Uninterruptable power supply (UPS)

For the control and monitoring system an uninterruptable power supply (UPS) with a back-up power supply is needed (class requirement). The standard power supply is 24 V DC but on demand another power supply is possible (e.g. 230 V AC or 480 V AC three phase current).

The engine control cabinet has an integrated voltage distribution for the control and monitoring systems at the engine (see fig. 13-3). Each cabinet has its DC/DC converter and its insolation monitoring device.

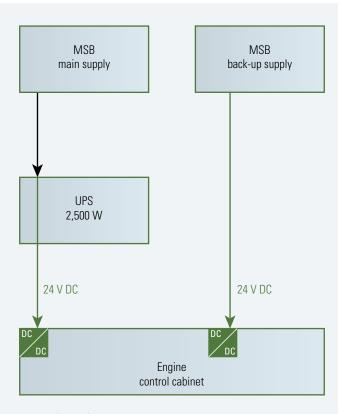


Fig. 13-6 Uninterruptable power supply - variants

13.7 Alarm indication

In general, the engine is equipped with the relevant alarm and safety sensorsaccording to classification society rules.

MACS provides an engine alarm system which is located in the local control panel. The engine alarm system and the local control display are consolidated in the DCU. The complete alarm management is handled by the DCU. All information is visualized via the screen in the LCP and additional several remote panels can be added.

The DCU receives measurement values and data from all I/O modules, PLC's and the engine control system (ECM). Furthermore it provides all measurement values, status values and alarm via MODbus TCP (MODbus RTU, optional) for the vessel's system and the remote monitoring system. The engine's alarm system determines critical engine conditions and activates alarms. The DCU has the ability of actuating the secondary safety stop valve. That means the DCU also works as well as a shut down unit and is able to stop the engine as reliable as the shut down unit (SDU). All alarms are stored in an alarm history and are shown in a manner requested by the MACS.







Fig. 13-8 DCU (display and alarm system)

For the interface to ship alarm system (IAMCS) the following functions are applicable:

- Transmitting measurement data to IAMCS
- Transmitting engine status to IAMCS
- Transmitting alarm to IAMCS
- Receiving ship's time stamp from IAMCS

All data is available via MODbus TCP. Upon request MODbus RTU is also possible. Device fault from the different MACS devices and some special alarms are provided as hardwired alarms.

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The table below shows an example of an overview of the different engine systems/modules with their safety functions.

A project related list of measurting points with all necessary MODbus information will be created for each order.

	IND/ FUNC	STBL	Alarm	ЭНЭ	SHD	GMI	SHOGE	SHOGM
Lube oil	Χ	Χ	Χ	X	Χ			0,
Oil mist detector	Х	Χ	Х		Χ			
Fresh water HT	Χ		Х		Χ			
Fresh water LT	Х		Х					
Air supply	Х	Χ	Х					
Charge air	Х		Х				Χ	
FCT	Χ		Х		Χ		Χ	
Electrical status	Х	Χ	Х			Х		
Engine status	Χ	Χ	Χ		Χ			
Combustion monitoring	X		Х		Χ	Х	Χ	
Exhaust gas	Χ		Χ	Χ			Χ	
Big end bearing	Χ		Χ		Χ			
Main bearing	X		Χ		Χ			
Load share unit (optional)			Χ		Χ			
ECM	X		Х				Χ	
Inert gas flushing	X					Х	Χ	Χ
Ignition fuel system engine	X	Χ	Х		Χ	Х	Χ	
Fuel gas system engine	Χ						Χ	
Fuel gas leakage monitoring	X		Х			Х	Χ	
Diesel gas mode control signals	X		X			Х	Χ	Χ
Gas valve unit	Χ		Χ			X	Χ	Χ
Ignition fuel module	Χ	Χ	Χ				Χ	
Crankcase gas detection	X		Χ				Χ	
Exhaust gas module	X	Χ			Χ	X	Χ	
Slow turn	Χ	Χ						
Ventilation modules	Χ							

Furthermore an evaluation of sensor faults is integrated. Depending on the importance of the failure it causes a STBL, E-STBL, CHG, GMI and SHOGE.

NOTE:

An active gas operation shut off (SHOGE/SHOGM) will activate gas mode interlock (GMI) and an engine shutdown will adtivate a starting interlock (STBL) as well as a gas shut off for the engine (SHOGE).

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FUNC Used in software function

IND Only for indication

A Alarm

STBL Starting interlock (overrideable by E-start of blackout start)

E-STBL Emergency starting interlock (not overrideable by E-start or blackout start)

CHG Change generator set

SHD Shutdown

GMI Gas mode interlock

SHOGE Gas shut off for engine / Shut off gas supply to engine.

The double block and bleed group in the gas valve unit (GVU) is closed.

SHOGMGas shut off for engine and machinery space.

The master gas valve has to be closed.

13.8 Local and remote indicators

Local indication	Remote indicators
Installed at the engine	96 x 96 mm (optional)
Fuel oil temperature at engine inlet	X ²⁾
Fuel oil differential pressure at filter	
Lube oil temperature at engine inlet	X ²⁾
Lube oil differential pressure at filter	
Fresh water temp. at engine inlet (HT circuit)	
Fresh water temp. at engine outlet (HT circuit)	X ²⁾
Fresh water temperature (LT circuit)	X ²⁾
Fresh water temperature cooler inlet	
Fresh water temperature cooler outlet	
Charge air temperature cooler inlet	
Charge air temperature engine inlet	X ²⁾
Fuel oil pressure	X ²⁾
Lube oil pressure	X ²⁾
Fresh water pressure (HT circuit)	X ²⁾
Fresh water pressure (LT circuit)	X ²⁾
Start air pressure	X ²⁾
Charge air pressure cooler outlet	X 2)
Stop air pressure	
Engine speed	X 1)
Turbocharger speed	X 1)
Charge air temp. cooler inlet (digital value)	
Exhaust gas temp. after cylinder (digital value)	
Exhaust gas temp. before / after turbocharger (digital value)	

1) 144 x 144 mm possible / 2) Signal is supplied by the alarm system

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13.9 Cat Connect for Marine provide by Caterpillar Marine Asset Intelligence (MAI)

MAI provides technology enabled solutions and services, that

- Provide remote monitoring and automated analytics via the internet.
- Combines equipment and application information.
- Applies predictive analytics.
- Utilizes interpretive expertise.

13.9.1 MAI - MaK engine solution only

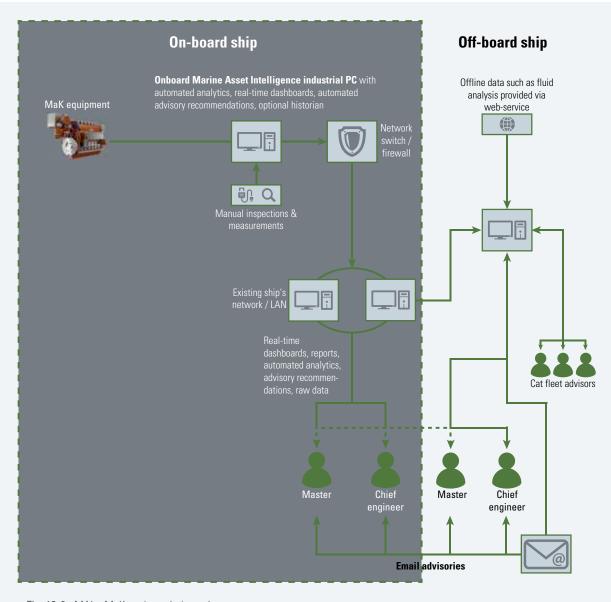


Fig. 13-9 MAI – MaK engine solution only

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13.9.2 MAI - Extended solution

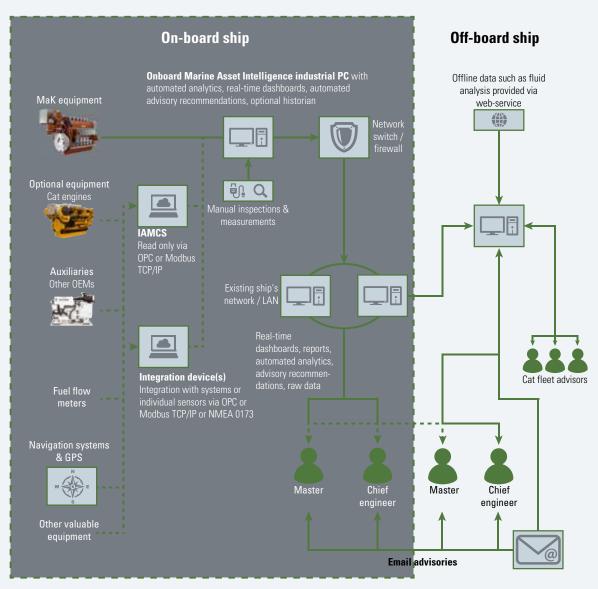


Fig. 13-10 MAI – Extended solution

13.9.3 General information

Capabilities

- Consolidates data and analyzes across all five condition monitoring elements.
- Analyzes data using multiple engines to identify and highlight exceptions.
- Creates a complete view of the equipment and performance.
- Allows more knowledgeable planned maintenance and scheduled repairs.
- Enables optimized tuning of equipment to maximize fuel efficiency.

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Comprehensive scope possible

- Monitors and analyzes variety of systems across the total vessel, based on what is important for each vessel.
- Can monitor Caterpillar/MaK equipment as well as non-Caterpillar/MaK equipment.
- Can monitor diesel engines and non-diesel engines.
- Primary services available:
 - Protect: Identify potential problems with equipment before there is a failure, assist onboard crew with remote expert troubleshooting.
 - Improve: Optimize fuel consumption for individual equipment through better maintenance and for entire vessel through operations and maintenance optimization.
 - Optimize: Move to condition based maintenance.
- Supporting services available:
 - Account: Ensure fuel accountability, measure and track fuel bunkering and consumption.
 - Save: Create visibility for unsafe operations or equipment condition.
 - Comply: Ensure equipment is operated and performs in compliance with regulations.
 - Manage: Customized dash-boards for different levels of management without custom software development.
 - Integrate: Integrate with other enterprise systems, such as Computerized Maintenance Management System (CMMS).

System Benefits

- Support most cost efficient operation.
- Provides optimized planning of service activities.
- Helps to avoid unexpected downtime.
- Helps reduce fuel cost for both the individual equipment and the entire vessel (depending on scope included).

Scope of delivery

- Electrical engine equipment MACS and Modbus interface for data streaming.
- Industrial PC with interfaces for connection to ship's network, automation system and other onboard systems.
- Software for real-time dashboard with online data view via ship's network (from any computer connected to ship's network).
- Network router with firewall for data replication via internet.
- Configuration of shore interface for shore customer users.
- Analytics with flexible reports and dashboards that can be configured and modified by the customer.
- Option: connection with additional systems beyond MaK/Caterpillar engines, to include other engines/ generators, auxiliary systems, other systems, individual sensors such as fuel flow sensors, torque meters, anemometers, GPS/ECDIS, etc via OPC, Modbus or NMEA data protocols.

Customer assumption

Network infrastructure and data transfer via satellite communication to be provided by customer.

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14.1 Safety

Potential operation Selected mode	Diesel operation	Gas operation
Diesel mode	Yes	No
Gas mode	Possible	Yes

"Mode" specifies the desired engine operation.

"Operation" specifies the actually burned fuel.

Fig. 14-1 Definition: "Mode" vs. "Operation"

Additional safety requirements need to be fulfilled to operate a dual fuel engine in a marine application. The safety concept for the MaK dual fuel engine is designed according the upcoming IGF code (draft international code of safety for ships using gases or other low-flashpoint fuels) to provide a gas safe machinery space.

14.1.1 Safety concept

The main intention of the safety concept is to avoid any hazardous situation. To this aim the safety concept for the dual fuel engine has to prevent the formation of any hazardous explosive atmosphere. Therefore a detection system is used in combination with automatic safety actions that will finally result in a changeover to diesel mode and flushing the fuel gas supply line with inert gas to avoid any endangering. Additionally a ventilation system for the exhaust pipe will inhibit an accumulation of fuel gas. Already during the design phase ignition sources have been considered and were excluded where possible.

To ensure highest level of safety CFD (Computational Fluid Dynamics) simulations were used and based on those data safety valves with sufficient relief areas were applied is necessary.

14.1.2 Gas safe machinery space

The safety concept for the dual fuel engine is based on a gas safe machinery space. The aim of this concept is that no hazardous atmosphere can occur in the machinery space. In case of any malfunction, the dual fuel engine will not shut down, instead the fuel supply will switch over to fuel oil as there are MDO and MGO. After reaching the diesel mode the engine can be switched over to HFO.

The switch over from fuel oil to fuel gas or vice versa will be bumpless and without any losses in power performance of the engine.

To avoid any hazardous area in the machinery space the fuel gas pipes in the machinery space are of double walled design from entering the engine room, via the gas valve unit throughout the cylinders. For detection of any leakage a suitable monitoring system is installed.

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SAFETY CONCEPT

To fulfill the requirements of a gas safe machinery room according to IMO resolution MSC.285(86) the following measures are taken:

- Fuel gas piping inside the machinery space must be of double walled design.
- All parts of the engine's fuel gas supply system inside the machinery space are double walled.
- The double wall is permanently monitored for leakage while the inner pipes are containing fuel gas.
- Flushing the fuel gas line with inert gas must be possible.
- Gas concentration must be monitored in the crankcase ventilation pipe.
- The lube oil system must be suitable for gas, class requirements have to be observed.
- The cooling water system must be suitable for gas, class requirements have to be observed.
- Means must be provided to inert and vent the crankcase for maintenance reasons.
- No direct access to gas hazardous areas must be possible.
- In case of a starting failure or an emergency shutdown of the engine while running on fuel gas the exhaust system will be ventilated automatically after emergency stop.
- In case of an emergency shutdown of the fuel gas supply or the engine, while the engine is running on fuel gas, the fuel gas supply lines will be flushed automatically with inert gas.
- Furthermore the system integrator needs to pay special attention to
 - The machinery room.
 - The gas handling room.
 - All rooms adjacent to possibly hazardous areas.

The engine control, monitoring and protection system, called MACS (Modular Alarm Control System), consists of different functional components. It includes the start-stop system, the gas management, the monitoring system and the engine protection system. A screen is fitted in the local control panel and shows measurement data as well as diagnostics and engine status.

14.1.3 Gas related safety equipment

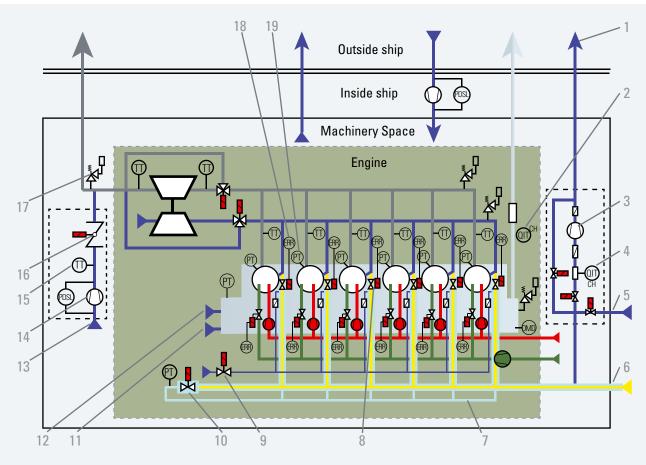


Fig. 14-2 Gas related safety equipment

1	Inertgas ventilation outlet	11	Crankcase flushing valve for inertgas
2	Gas sensor in crankcase ventilation line	12	Crankcase purging valve for compressed air
3	Vacuum pump in ventilation module	13	Air inlet for exhaust gas duct purging
4	Gas sensor in ventilation module	14	Fan for exhaust gas duct purging
5	Inertgas supply inlet	15	Temperature transmitter
6	Fuel gas supply	16	Butterfly isolation valve
7	Inertgas compartment	17	Explosion relief valve
8	GAV (Gas Admission Valve)	18	In cylinder pressure sensor
9	Fresh air flushing valve	19	In cylinder pressure transmitter
10	Inertgas flushing valve		

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INSTALLATION AND ARRANGEMENT

15.1 Resilient mounting of genset

Basic design and arrangement

The engine is resiliently mounted on the baseframe and all pipe connections to the baseframe are flexible. The generator is connected with the engine via a high flexible coupling and rigidly mounted on the baseframe. This design ensures high vibration isolation between engine and the baseframe generator arrangement.

The resilient mounting arrangement of the engine is designed to reach the best possible load distribution of the engine weight in respect of the maximal permissible deflection of the conical rubber element. The whole genset is rigidly connected with the vessel's foundation via bolts. The vessels' foundation itself does not require machining, but unevenness between the baseframe and the foundation has to be compensated either using welded-on sheets and shims or resin chocks.

15.1.1 Conical mountings

General

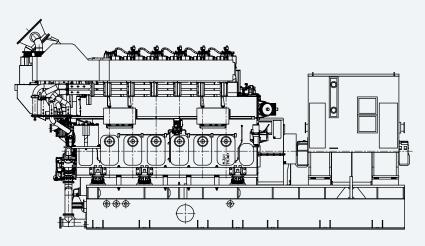
The used conical design provides high deflection and load capacity combined with long service life. The life expectancy of the rubber elements will be approx. 20 years in ideal circumstances. In fact of bad influences out of environmental circumstances the (working) life expectancy will be approx. 10 years.

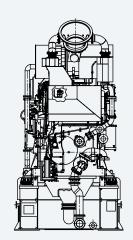
Specifications

The used conical mountings have been approved from all relevant classification societies. All mounting rubber inserts are individual tested and selected on stiffness by our supplier.

An adjustable central buffer controls the mounted equipment displacements due to ship movements vertically and horizontally within defined limits.









INSTALLATION AND ARRANGEMENT

15.2 Earthing of engine

Information about the execution of the earthing

The earthing has to be carried out by the shipyard during the assembly on board.

The engine is already equipped with M 16, 25 mm deep threaded holes in the lower part of the baseframe.

If the engine is resiliently mounted it is important to use flexible conductors.

In case of using welding equipment it is important to earth the welding equipment close to the welding area (the distance should not exceed 10 m).

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16.1 Data for torsional vibration calculation

To determine the location and resonance points of each engine and equipment Caterpillar Motoren calculates the torsional vibration behaviour of the engine, including all components, such as coupling, gearboxes, shaft lines and propellers, pumps, and generators.

The normal as well as the emergency operating mode is covered.

The classification societies require a complete torsional vibration calculation.

To be able to provide a correct torsional vibration calculation, we would like to ask you to fill in the documents in the appendix, according to your scope of supply.

Please send the completed data to your local dealer 6 month prior to the engine delivery at the latest. For further information please compare the data sheet for torsional vibration calculation. (following 3 pages).

CAT°	☐ Main driv	e Shipya	rd:	<u></u>	
	Aux. Eng	ine Shipow	ner:	<u></u>	
Additional engine	□ DE drive	Type of	vessel:		
plant data part "B"	KtrNo.:	Newbu	Iding No.:		
Remark:					
Please note that the appl after receiving the complete plant data sheet" part "A"	ted "Addition	al engine plant data	a sheet" part		
General information, re	quired for a	II applications:			
Flag state (needed for EIAF	PP cert):				
Certificate" as per flag state weeks prior to the engine d has not been provided to C Statement of Compliance" of Certificate" as per flag state conversion has to be borne	elivery date as aterpillar Moto which has to be authorization	s per the Sales Con oren until such date, be converted into "E a. In this case the ap	tract (Append Caterpillar N APP Docume	dix 1). In case such i Notoren will provide a ents of Compliance"	nformation an "EAPP or an "EIAPP
Alarm system					
yard maker:	type	e: yard	contact mana	ager:	
Make of automation/bus s	system				
yard maker:	type	e: yard	contact mana	ager:	
Additional information	for cooling v	water system:			
Add. heat exchanger integrate number of aux. engine		, Yes No, if "	Yes " please pro	ovide the following dat	a:
☐ heat dissipation ☐		required water flow number of cooler _	,	pressure drop _	bar
heat dissipation		required water flow		pressure drop _	bar
air cond. unit		number of air cond.	unit		
heat dissipation	kW	required water flow	m³/h	pressure drop _	bar
others		lease specify:			
heat dissipation	kW	required water flow	m³/h	pressure drop _	bar
Comments/Remarks:					
Caterpillar Confidential: Green					

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Fig. 16-1 Additional engine plant data, part "B" (1/3)

CAT°	Additional e	ngine pl	ant data, part "B"
TVC data - Information fo	r main engine(s) oı	nl <u>y</u> :	
Flex. coupling main engine:			
Supplied by Caterpillar Yes	No, if " No" please	provide the f	ollowing data:
☐ Vulkan Type:	☐ Stromag Size: ☐ Drawing atta	ched	☐ Centa ☐ TVC scheme attached ☐ Drawing attached
Other maker	_		_
Type:	Size:		☐ TVC scheme attached☐ Drawing attached
Norminal torque [kNm]: Perm. power loss [kW]:			vibratory torque [kNm]:
Dyn. torsinal stiffness[kNn	n/rad]:		otational speed [1/min]: e damping:
Flex. coupling engine PTO sha	ft (on engine free-end)	
Supplied by Caterpillar Yes	☐ Not applicable	☐ No, if " <u>I</u>	No " please provide the following data:
□ Vulkan	Stromag		Centa
Type:	Size: ☐ Drawing atta	ched	
Other maker			
Type:	Size:		
Norminal torque [kNm]:			vibratory torque [kNm]:
Perm. power loss [kW]: Dyn. torsinal stiffness[kNm	n/rad]:		otational speed [1/min]: e damping:
Flex. coupling gearbox PTO			
Supplied by Caterpillar Yes	☐ Not applicable	☐ No, if " I	<u>No</u> " please provide the following data:
☐ <u>V</u> ulkan	☐ Stromag		Centa
Туре:	Size: ☐ Drawing atta	ched	☐ TVC scheme attached☐ Drawing attached
Other maker			
Type:	Size:		☐ TVC scheme attached ☐ Drawing attached
Norminal torque [kNm]:			vibratory torque [kNm]:
Perm. power loss [kW]: Dyn. torsinal stiffness[kNm	n/rad]:		otational speed [1/min]: e damping:
Gearbox		· totaliv	
Supplied by Caterpillar Yes	☐ No, if " No " please	provide the f	ollowing data:
Maker:			☐ TVC scheme attached
Max. permissible PTO output			☐ Drawing attached
Front gearbox for engine PTO	_	_	
Supplied by Caterpillar Yes	☐ Not applicable	☐ No, if " I	No" please provide the following data:
Maker: Max. permissible PTO output	Type: [kW]:		☐ TVC scheme attached☐ Drawing attached
PTO shaft generator/fire fightii	ng pump or similar cor	nsumer, dri	ven by engine PTO shaft/front step up gear
Supplied by Caterpillar Yes	☐ Not applicable	☐ No, if " <u>I</u>	No " please provide the following data:
Maker: Output [kW]:	Type: rpm [1/min]:		☐ TVC scheme attached
Plain bearing, external lub	rication		Drawing attached
Caterpillar Confidential: Green			

Fig. 16-2 Additional engine plant data, part "B" (2/3)

	Additional engine plant data, part "B"
TVC data	- Information for main engine(s) only:
PTO shaft g	enerator, driven via gearbox
Supplied by	Caterpillar Yes Not applicable No, if " No please provide the following data:
Maker:	
	VA]: rpm [1/min]: TVC scheme attached
☐ PTI op	peration PTI output [kW]:
Shaft arrang	gement between engine - gearbox
Supplied by	Caterpillar Yes No, if " <u>No</u> " please provide the following data:
Maker:	TVC scheme attached detail drawing:
Propeller an	d propeller shafting data:
Supplied by	Caterpillar Yes No, if " No " please provide the following data:
☐ CPP	☐ FPP ☐ Voith ☐ Rudder FPP/CPP ☐ Others
numbers	of blades: Ø propeller [mm]:
Moments	of inertia in water [kgm²]: Moments of inertia in air [kgm²]:
Maker:	TVC scheme attached or detail drawing:
Dramallar ar	d annuallar abaddina information.
	nd propeller shafting information: Caterpillar No Yes, in case of "Yes" please provide the following data:
□ wake	field attached
	(
Comments/I	Remarks:
	Remarks:
Confirmed by	
Confirmed by	
Confirmed by	y buyer:
	y buyer:
Confirmed by	y buyer:
Confirmed by	y buyer:
Confirmed by Date:	y buyer:
Confirmed by Date: Stamp and s Caterpillar ca	y buyer:ignature:
Confirmed by Date: Stamp and s Caterpillar cate	buyer: ginature: annot be held liable for any mistakes made by the buyer. not mentioned in Cat's technical specification/No, dd and essential for peration of the equipment will be buyer's scope of supply.
Confirmed by Date: Stamp and s Components installation/o	buyer: ginature: annot be held liable for any mistakes made by the buyer. not mentioned in Cat's technical specification/No, dd and essential for



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16.2 Sound levels

16.2.1 Airborne noise

The airborne noise level requirement in the engine room specified by IMO Resolution A.468 will be satisfied by M 46 DF (even for multiple installations).

The airborne noise level is measured in a test cell according to EN ISO 9614-2.

16.3 Vibration

The vibration level of M 46 DF engines complies with ISO 20283-4 and ISO 10816-6.

From these ISO standards, the following values are an applicable guideline:

17.1 Flexible coupling

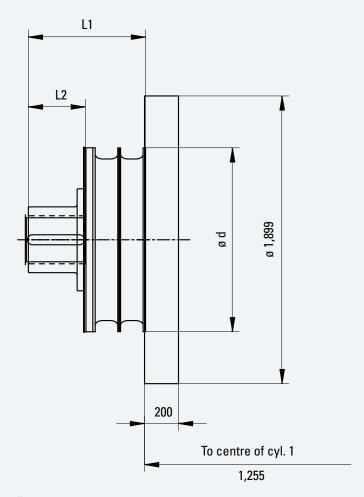


Fig. 17-1 Flexible coupling

	Power	Speed	Nominal torque of				Weight	
	I OWEI	Speeu	coupling	d	L1 ²⁾	L2 1)	vveigiit	
	[kW]	[rpm]	[kNm]	[mm]	[mm]	[mm]	[kg]	
6 M 46 DF	5,400 5,790*)	500/514	125	1,240	729	385	1,200	
7 M 46 DF	6,300 6,755*)	500/514	160	1,240	745	385	1,500	
8 M 46 DF	7,200 7,720*)	500/514	160	1,240	745	385	1,500	
9 M 46 DF	8,100 8,685*)	500/514	200	1,460	954	480	2,100	

 $^{^{*)}}$ MDO operation only /1) Length of hub / 2) Alignment control (recess depth 8 mm)

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PIPING DESIGN

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18.1 Pipe dimensions

The external piping systems are to be installed and connected to the engine by the shipyard.

Piping systems are to be designed so as to keep the pressure losses at a reasonable level.

To achieve this at justifiable costs, it is recommended to keep flow rates as indicated below (see chapter 18.2).

Nevertheless, depending on specific conditions of piping systems, it may be necessary to adopt even lower flow rates.

ATTENTION:

Generally it is not recommended to adopt higher flow rates.

18.2 Flow velocities in pipes

	Recommended flow rates [m/s]				
	Suction side	Delivery side	Kind of system		
Fresh water (cooling water)	1.5 - 3.0	1.5 - 3.0	Closed		
Lube oil	0.5 - 1.0	1.5 - 2.5	Open		
Sea water	1.0 - 1.5	1.5 - 2.5	Open		
Diesel fuel oil	0.5 - 1.0	1.5 - 2.5	Open		
Heavy fuel oil	0.3 - 0.8	1.0 - 1.5	Open / closed pressurized system		
Exhaust gas	20 - 40		Open		

18.3 Trace heating

Trace heating is highly recommended for all pipes carrying HFO or leak oil. For detailed explanation see fuel oil diagrams, showing the trace heated pipes marked as

18.4 Insulation

All pipes with a surface temperature > 60 °C should be insulated to avoid risk of physical injury.

This applies especially to exhaust gas piping.

To avoid thermal loss, all trace heated pipes should be insulated.

Additionally, lube oil circulating pipes, the piping between engine and lube oil separator as well as the cooling water pipes between engine and preheater set should be insulated.

PIPING DESIGN

18.5 Flexible pipe connections

Flexible pipe connections become necessary to connect resilient mounted engines with external piping systems. these components have to compensate the dynamic movements of the engine in relation to the external piping system.

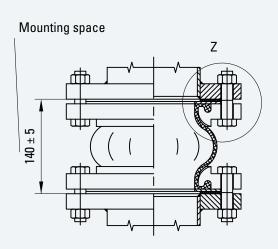
The shipyard's pipe system must be exactly arranged so that the flanges or screw connections fit without lateral or angular offset. It is recommended to adjust the final position of the pipe connections after engine alignment is completed.

It is important to support as close as possible to the flex connection and stronger than normal. The pipes outside the flexible connection must be well fixed and clamped to prevent from vibrations, which could damage the flexible connections.

Installation of steel compensators

Steel compensators can compensate movements in line and transversal to their center line. They are not suitable for compensating twisting movements. Compensators are very stiff against torsion.

It is very important that all steel compensators are not allowed to be installed on resilient mounted engines in vertical direction.





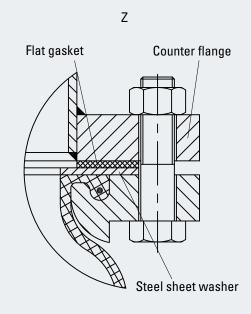


Fig. 18-2 Rubber expansion joint, detail Z

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19.1 Genset center distances

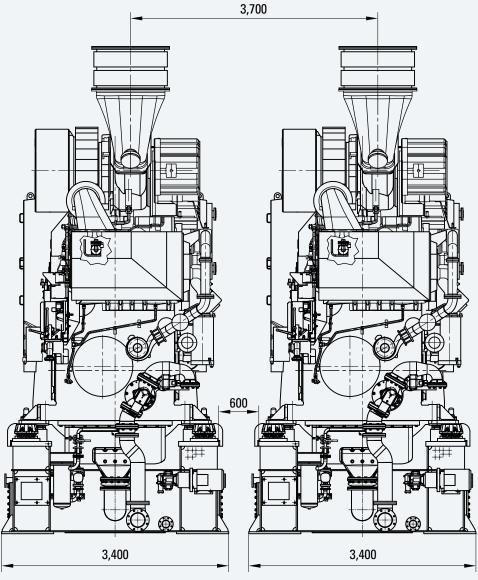
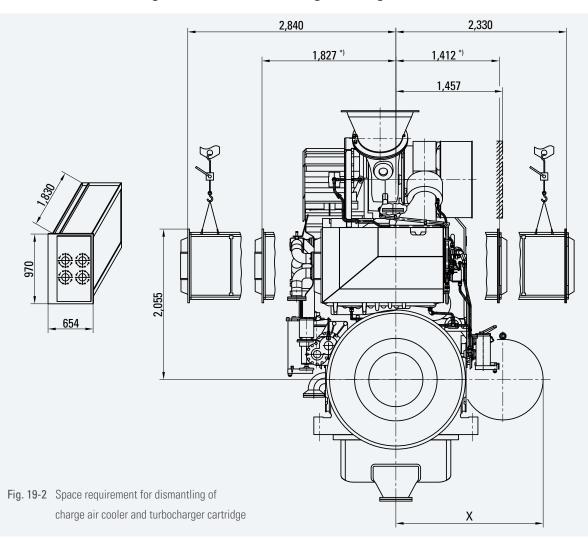


Fig. 19-1 Center distance of twin-engine plants

Type	Dimensions [mm]		
lype	А		
6/7/8/9 M 46 DF	3,700		

19.2 Space requirement for maintenance

19.2.1 Removal of charge air cooler and turbocharger cartridge



Туре	Weight charge air cooler [kg]	Weight turbocharger cartridge [kg]
6 M 46 DF	1,138	460
7/8/9 M 46 DF	1,124	820

Type	Damper ø	Weight	Χ
туре	[mm]	[kg]	[mm]
6 M 46 DF	1,100	960	2,010
7 M 46 DF	1,340	1,538	2,250
8 M 46 DF	1,480	2,527	2,390
9 M 46 DF	1,480	2,527	2,390

^{*)} Splitted charge air cooler

Charge air cooler cleaning

Cleaning is carried out with charge air cooler dismantled. A container to receive the cooler and cleaning liquid is to be supplied by the yard. Intensive cleaning is achieved by using ultra sonic vibrators.

Turbocharger dismantling

To provide a lifting rail with a travelling trolley right above the center of the turbocharger in order to carry out scheduled maintenance work is recommended...

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19.2.2 Removal of piston and cylinder liner

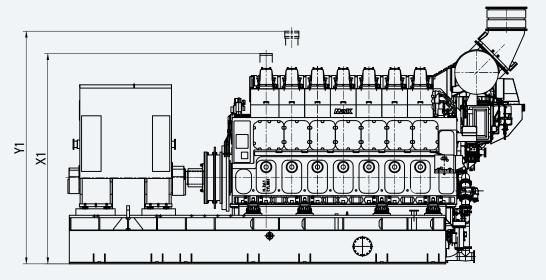


Fig. 19-3 Removal of piston and cylinder liner

Removal of:

Piston: in transverse direction X1 = 5,974 mm

Cylinder liner: in transverse direction Y1 = 6,609 mm

20.1 Inside preservation

20.1.1 Factory standard N 576-3.3 – Inside preservation

Components

Main running gear and internal mechanics

Application

• Max. 2 years

NOTE:

Inside preservation does not have to be removed when the engine is commissioned.

20.2 Outside preservation

20.2.1 Factory standard N 576-3.2 – Outside preservation VCI 368

Conditions

- Europe and overseas
- Sea and land transportation
- Storage in the open, protected from moisture max. 2 years with additional VCI packaging

Appearance of the engine

- · Castings with red oxide antirust paint
- Pipes and machined surfaces left as bare metal
- Attached components with colours of the manufacturers

NOTE:

Outside preservation must be removed before commissioning of the engines.

Environmentally compatible disposal is to be ensured.

Durability and effect depend on proper packaging, transportation, and storage (i.e. protected from moisture, stored at a dry place and sufficiently ventilated). Inspections are to be carried out at regular intervals.

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20.2.2 Factory standard N 576-4.1 – Clear varnish

Conditions

- Europe
- Roofed land transportation
- Storage in a dry and tempered atmosphere, protected from moisture max. 1 year with additional VCI packaging

NOTE:

Clear varnish is not permissible for sea transportation of engine and storage of engines in the open, even if they are covered with tarpaulin.

Appearance of the engine

- · Castings with red oxide antirust paint
- Pipes and machined surfaces left as bare metal
- Attached components with colours of the manufacturers
- Surfaces sealed with clear varnish
- Bare metal surfaces provided with VCI 368 preservation

NOTE:

VCI packaging as per factory standard N 576-5.2 is generally required!

Durability and effect depend on proper packaging, transportation, and storage (i.e. the engine is to be protected from moisture, VCI film not ripped or destroyed).

Inspections are to be carried out at regular intervals.

If the above requirements are not met, all warranty claims in connection with corrosion damage shall be excluded.



20.2.3 Factory standard N 576-4.3 – Painting

Conditions

- Europe and overseas
- Sea and land transportation
- Short-term storage in the open, protected from moisture up to max. 4 weeks
- Longer than 4 weeks VCI packaging as per factory standard N 576-5.2 is required
- Max. 2 years with additional VCI packaging

Appearance of the engine

- Surfaces mostly painted with varnish
- Bare metal surfaces provided with VCI 368 preservation

NOTE:

Durability and effect depend on proper packaging, transportation, and storage (i.e. the engine is to be protected from moisture, VCI film not ripped or destroyed).

Inspections are to be carried out at regular intervals.

20.2.4 Factory standard N 576-5.2 – VCI packaging

Conditions

- Engines with outside preservation VCI 368 as per factory standard N 576-3.2
- Engines with clear varnish as per factory standard N 576-4.1

NOTE:

These engines are always to be delivered with VCI packaging! Nevertheless, they are not suitable for storage in the open!

- Engine or engine generator sets with painting as per factory standard N 576-4.3
- Europe and overseas
- Storage in the open, protected from moisture

NOTE:

Durability and effect depend on proper packaging, transportation, and storage (i.e. the engine is to be protected from moisture, VCI film not ripped or destroyed).

Inspections are to be carried out at regular intervals.

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Apperance of the engine

- Bare metal surfaces provided with VCI 368 or VCI oil
- VCI impregnated flexible PU foam mats attached to the engine using tie wraps.
 Kind and scope depending on engine type.

The attached mats should not come into contact with the painted surface.

Cover the engine completely with air cushion film VCI 126 LP. Air cushions are to face inwards!
 The air cushion film is fastened to the transportation skid (wooden frame) by means of wooden laths.
 Overlaps at the face ends and openings for the lifting gear are to be closed by means of PVC scotch tape. In case of engines delivered without oil pan, the overhanging VCI film between engine and transport frame is to be folded back upwards before fastening the air cushion film.

ATTENTION:

The corrosion protection is only effective if the engine is completely wrapped in VCI film. The protective space thus formed around the component can be openend for a short time by slitting the film, but afterwards it must be closed again with adhesive tape.

20.2.5 Factory standard N 576-5.2 Suppl. 1 – Information panel for VCI preservation and inspection

An information panel for VCI preservation and inspection will be supplied.

Application

Engines with VCI packaging as per factory standard N 576-5.2

Description

- This panel provides information on initial preservation and instructions for inspection.
- Arranged on the transport frame on each side so as to be easily visible.

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20.3 Factory standard N 576-6-1 – Protection period, check, and represervation

20.3.1 Protection period

There will only be an effective corrosion protection of the engine if the definitions and required work according to factory standard N 576-6.1 are duly complied with.

Normally, the applied corrosion protection is effective for a period of max. 2 years, if the engine or engine generator set is protected from moisture.

After two years represervation must be carried out.

However, depending on the execution of the preservation or local conditions shorter periods may be recommended

20.3.2 Protection check

Every 3 months specific inspections of the engine or engine generator set are to be carried out at defined inspection points.

Any corrosion and existing condensation water are to be removed immediately.

20.3.3 Represervation as per factory standard N 576-6.1

After 2 years represervation must be carried out.

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TRANSPORT, DIMENSIONS AND WEIGHTS

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Lifting of engines 21.1

For more information regarding the lifting of the engine, please contact Caterpillar Motoren.

Dimensions of main components 21.2

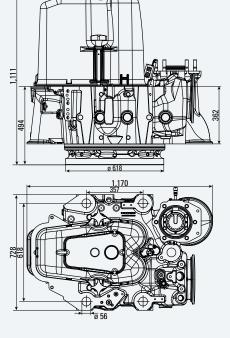


Fig. 21-1 Cylinder head (2D), weight 1,147 kg

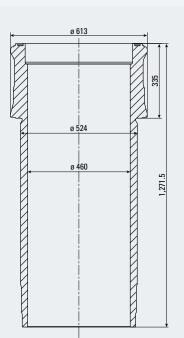


Fig. 21-3 Cylinder liner (2D), weight 560 kg



Fig. 21-2 Cylinder head (3D)



Fig. 21-4 Cylinder liner (3D)

TRANSPORT, DIMENSIONS AND WEIGHTS

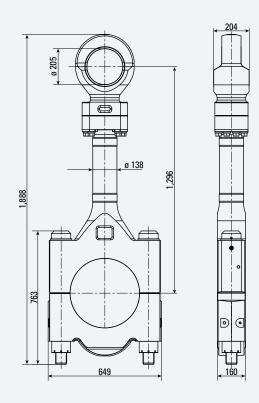


Fig. 22-5 Connecting rod (2D), weight 560 kg



Fig. 22-6 Connecting rod (3D)

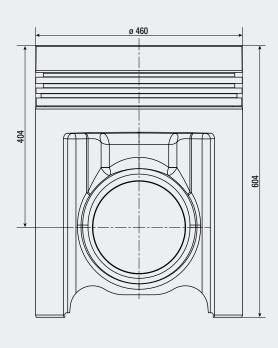


Fig. 22-7 Piston (2D), weight 230 kg



Fig. 22-8 Piston (3D)

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STANDARD ENGINE ACCEPTANCE TEST RUN

22.1 Standard acceptance test run

The acceptance test run is carried out on the testing bed with customary equipment and auxiliaries using exclusively MDO and under the respective ambient conditions of the testing bed. During this test run the fuel rack will be blocked at the contractual output value. In case of deviations from the contractual ambient conditions the fuel consumption will be converted to standard reference conditions. The engine will be run at the following load stages according to the rules of the classification societies.

Diesel mode

Load [%]	Duration [min]
Diesel mode	
25	20
50	20
75	20
85	20
100	60
110	30
Gas mode	
25	20
50	20
75	20
85	20
100	60

The load stages above can vary according to the requirements of the classification societies.

After reaching steady state conditions of pressures and temperatures these will be recorded and registered according to the form sheet of the acceptance test certificate.

Additional functional tests

In addition to the acceptance test run the following functional tests will be carried out:

- Governor test
- Overspeed test
- Emergency shut-down via minimum oil pressure
- Start/stop via central engine control
- Starting trials up to a minimum air pressure of 10 bar
- Measurement of crank web deflection (cold/warm condition)

After the acceptance, main running gear, camshaft drive and timing gear train will be inspected through the opened covers. Individual inspection of special engine components such as piston or bearings is not intended, because such inspections are carried out by the classification societies at intervals on series engines.

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23.1 Required spare parts (Marine Classification Society MCS)

Classification societies	GL	RS	KR	ccs
Rules references	Pt. 1, Ch. 17	Pt. 7, Ch. 10	Pt. 5, Ch. 1	Ch. 15, Sec. 1&2
Parts				
Main bearing	1	1	1	1
Thrust washer	1	1	1	1
Cylinder liner, complete	1	1	1	1
Cylinder head, complete	1	1	1	1
Cylinder head, only with valves (w/o injection valve)	_	_	_	_
Set of gaskets for one cylinder head	_	_	_	_
Set bolts and nuts for cylinder head	1/2	1/2	1/2	1/2
Set of exhaust valves for one cylinder head	1	(2)*	2	2
Set of intake valves for one cylinder head	1	(1)*	1	1
Starting air valve, complete	1	1	1	1
Relief valve, complete	1	1	1	1
Injection valve, complete	_	_	_	_
Set of injection valves, complete, for one engine	1	1	1	1
Set of conrod top & bottom bearing for one cylinder	1	1	1	1
Piston, complete	1	1	1	1
Piston, without piston pin + piston rings	_	_	_	_
Connecting rod	1	1	1	1
Big end bearing	_	_	_	_
Gudgeon pin with bushing for one cylinder	1	1	1	1
Set of piston rings	1	1	1	1
Fuel injection pump	1	1	1	1
Fuel injection piping	1	1	1	1
Set of gaskets and packing for one cylinder	1	1	1	1
Exhaust compensators between cylinders	1	_	1	1
Turbocharger rotor, complete	_	(1)*	_	_
Set of gear wheels	_	_	_	_
ECU	1	1	1	1
Speed pick up camshaft	1	1	1	1
Speed pick up crankshaft	1	1	1	1
DCU	1	_	_	_
Only for electronic speed setting Pick up for electronic speed setting	_	_	_	_
Only if oil mist detector is provided Sintered bronze filter (for crankcase monitor)	_	_	_	_

^{*} Recommendation only

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* Recommendation only / ** Owner's responsibility

23.2 Recommended spare parts

Classification societies	ABS	DNV	LR	BV **	RINA **
Rules references	Pt. 4, Ch. 2 Sec. 1	Pt. 4, Ch. 1, Sec. 5	Pt. 5, Ch. 16, Sec. 1	Pt. A, Ch. 1, Sec. 1	Pt. A, Ch. 1, Sec. 1
Parts	1	1	1	1	'
Main bearing	1	1	1	_	_
Thrust washer	1	1	1	_	_
Cylinder liner, complete	1	_	1	_	_
Cylinder head, complete	1	_	1	_	_
Cylinder head, only with valves (w/o injection valve)	_	_	_	_	_
Set of gaskets for one cylinder head	_	_	_	_	_
Set bolts and nuts for cylinder head	1/2	_	1/2	_	_
Set of exhaust valves for one cylinder head	2	2	2	_	_
Set of intake valves for one cylinder head	1	1	1	_	_
Starting air valve, complete	1	1	1	_	_
Relief valve, complete	1	1	1	_	_
Injection valve, complete	_	_	_	_	_
Set of injection valves, complete, for one engine	1	1/2	1	_	_
Set of conrod top & bottom bearing for one cylinder	1	1	1	_	_
Piston, complete	1	_	1	_	_
Piston, without piston pin + piston rings	_	_	_	_	_
Connecting rod	1	_	1	_	_
Big end bearing	_	_	_	_	_
Gudgeon pin with bushing for one cylinder	1	1	1	_	_
Set of piston rings	1	1	1	_	_
Fuel injection pump	1	1	1	_	_
Fuel injection piping	1	1	1	_	_
Set of gaskets and packing for one cylinder	1	1	1	_	_
Exhaust compensators between cylinders	1	_	1	_	_
Turbocharger rotor, complete	_	_	_	_	_
Set of gear wheels	1	_	_	_	_
ECU	1	1	1	1	1
Speed pick up camshaft	1	1	1	1	1
Speed pick up crankshaft	1	1	1	1	1
Only for electronic speed setting Pick up for electronic speed setting	_	_	_	_	_
Only if oil mist detector is provided Sintered bronze filter (for crankcase monitor)	_	_	_	_	_



ENGINE PARTS

Caterpillar recommendation	Caterpillar
Rules references	Gator pinar
Parts	
Main bearing	1
Thrust washer	_
Cylinder liner, complete	1
Cylinder head, complete	_
Cylinder head, only with valves (w/o injection valve)	1
Set of gaskets for one cylinder head	1
Set bolts and nuts for cylinder head	1/2
Set of exhaust valves for one cylinder head	_
Set of intake valves for one cylinder head	_
Starting air valve, complete	_
Relief valve, complete	_
Injection valve, complete	1
Set of injection valves, complete, for one engine	_
Set of conrod top & bottom bearing for one cylinder	_
Piston, complete	-
Piston, without piston pin + piston rings	1
Connecting rod	_
Big end bearing	1
Gudgeon pin with bushing for one cylinder	_
Set of piston rings	1
Fuel injection pump	1
Fuel injection piping	1
Set of gaskets and packing for one cylinder	_
Exhaust compensators between cylinders	1
Turbocharger rotor, complete	_
Set of gear wheels	_
ECU	1
Speed pick up camshaft	1
Speed pick up crankshaft	1
DCU	1
Gas admission valve	2
Ignition injector	2
Cylinder pressure sensor	1
Set of dual fuel gaskets	1
Rail pressure sensor	1
Gas compensator	1
Ignition fuel high pressure pump	1

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CATERPILLAR MARINE

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24.1 Gas systems technology – Scope of supply

Beside the gas / dual fuel engines itself Caterpillar offers also the whole gas system which is needed to operate the engine onboard the vessel.

Whether on a new building or for a retrofit project, the service can include:

- Gas / dual fuel engines
- FEED study (Front End Engineering and Design study)
- A&I engineering
- Bunker station
- LNG storage tank
- Gas handling system
- Gas and LNG piping
- Gas valve unit
- Control & monitoring
- Safety systems

The customer can benefit from getting a whole solution from one hand. Supported by our strong dealer and customer support organizations.

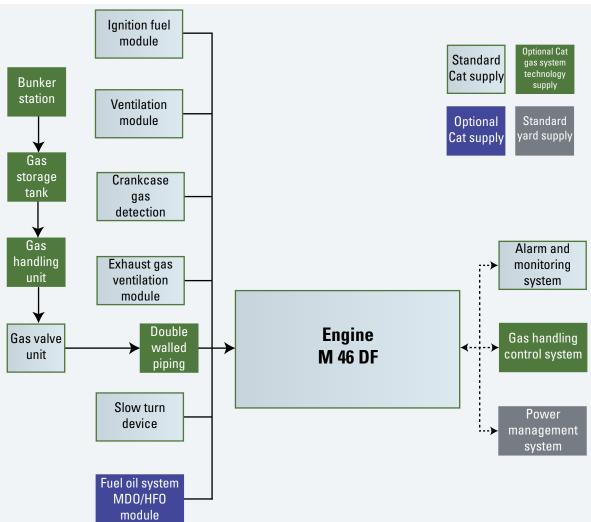


Fig. 24-1 Scope of supply M 34 DF Gas systems technology – block diagram

CATERPILLAR MARINE

24.2 Caterpillar Propulsion

Performance You Can Rely On

Caterpillar Propulsion supplies complete, world-leading propulsion systems.

Custom-designed and optimized for uptime and cost-effective operations, our top-of-the-line controllable pitch propellers, thrusters, control systems, and hubs are all manufactured at our state-of-the-art production facilities in Sweden and Singapore.



Fig. 24-2 Controllable pitch propeller

We are experts in innovative hydrodynamics to ensure heavy-duty, reliable performance for our customers.

How we deliver uptime

Our guiding principle is to deliver maximum uptime for our customers' peace-of-mind and profitability.

For us, this means using more material to ensure our propulsion systems are built to last even in the most extreme conditions. And with extreme attention to detail, we study your vessel's design, the job at hand – anything and everything that affects the hydrodynamics.

Using all our expertise, we're not finished until the system is as optimized and reliable as possible. Please visit us at catpropulsion.com.



Fig. 24-3 Azimuth thrusters



Fig. 24-4 Tunnel thrusters



Fig. 24-5 Remote control system

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The Power You Need.

The Cat® and MaK™ brands of Caterpillar Marine offer premier high- and medium-speed propulsion, auxiliary, and generator set solutions, as well as optional dual fuel, diesel-electric, and hybrid system configurations. With the launch of Caterpillar Propulsion our comprehensive and evolving product line gives customers one source for the most extensive engine power range available, complete propulsion systems, controllable pitch propellers, transverse and azimuth thrusters, and controls. Cat and MaK products and technologies are proven reliable and are built to last in all marine applications, demonstrating superior productivity and the lowest lifecycle cost.

The Cat Global Dealer Network, more than 2,200 global service locations strong, ensures that you'll have local expertise, highly-trained technicians, rapid parts delivery, and the proper equipment and services to keep you working — anytime, anywhere.

Construction, term, or repower financing through Cat Financial helps you make Cat and MaK power a reality. With our knowledge of customer needs, local markets, and legal and regulatory requirements, we've been providing tailored financing solutions and exceeding expectations since our start in 1986.

For more information and to find your local dealer, please visit our website: **www.cat.com/marine**Visit Cat Financial at: **CatPowerFinance.com**

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Europe, Africa, Middle East Americas Asia Pacific

MaK Americas Inc.

Caterpillar Marine A Division of Caterpillar Motoren GmbH & Co. KG Neumühlen 9 22763 Hamburg Germany

+49 40 2380-3000

+49 40 2380-3535

Phone:

Telefax.

763 Hamburg Miramar Park of Commerce many Miramar, FL. 33025/USA

Please check out for more

3450 Executive Way
25/F, Caterpillar Marine Center
Miramar Park of Commerce
1319, Yan'an West Road
Miramar, FL. 33025/USA
200050 Shanghai/P.R. China

Phone: +1 954 885 3200 Phone: +86 21 6226 2200 Phone: +65 68287-600
Telefax: +1 954 885 3131 Telefax: +86 21 6226 4500 Telefax: +65 68287-625

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Caterpillar Marine Asia

Pacific Pte Ltd.

Innovation Grove

Singapore 618304

Republic of Singapore

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